

Evaluation Of Inside Heat Transfer Coefficient of Roll Bond Evaporator for Room Air Conditioner

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ABSTRACT: In all refrigeration and air conditioning equipment the evaporator is either a plate and fin evaporator, tube and fin or a plate and tubular evaporator. There were little changes in manufacturing methods and geometry. This paper presents a new design of evaporator, in which roll bond evaporator is used in room air conditioner. Presently the use of roll bond evaporator is limited to domestic refrigerators only. The study throws light on evaluating the inside heat transfer coefficient (refrigerant side) of the roll bonded evaporator using R-22 as Refrigerant

KEYWORDS: Roll bond evaporator, R- 22, Weld Stop, ASHRAE

I. INTRODUCTION

In the pursuit of reducing global warming, the world is looking for the methods of reducing energy consumption. In India, appliances working on refrigeration system are one of the major contributing factors to energy consumption. With changing life style and increased standard of living the energy consumption is steadily increasing. Studies have been conducted to reduce the energy consumption by developing higher efficiency products. In a Refrigeration and Air conditioning system, major part of the energy is wasted by the system components compressor, condenser, evaporator and capillary tube due to irreversible processes. The thermodynamic study of these parts has emphasised the need to develop higher efficiency products. A house hold refrigerator or even a room air conditioner has to be designed so as to reduce the losses. In his studies, Jakobsen [1] has concluded that the losses in a Refrigeration and Air conditioning system are mainly in compressor and in the evaporator. In India, the most widely used evaporator in refrigerators is either a plate and tube evaporator or a roll bond evaporator. In air conditioners, tube and fin evaporator is widely used. In this study, roll bond evaporator is used in room air conditioner instead of tube and fin evaporator. The heat transfer characteristics of the refrigerant (inside heat transfer coefficient refrigerant side) is evaluated.

Roll bond evaporators deliver efficient thermal performance. It evaporator is fabricated by rolling together two sheets of aluminum applying heat and pressure during the rolling process such that the two sheets are effectively welded together into a single sheet. By applying special coating called "weld stop" or a chemical ink between the sheets prior to the rolling/welding operation, it is possible to prevent the two sheets from welding together in the areas where the coating is applied.

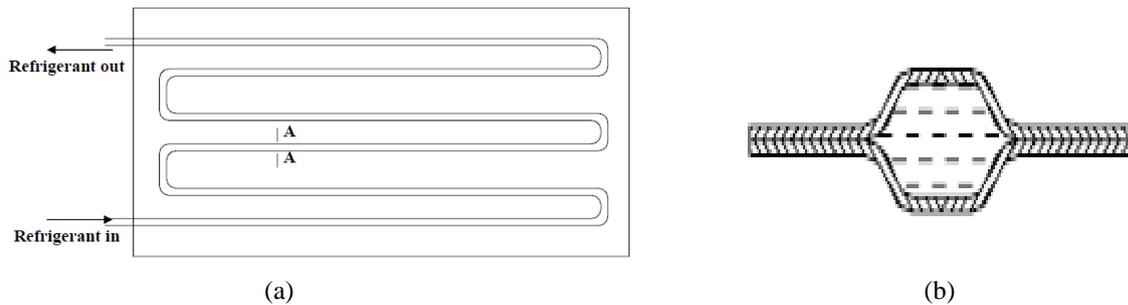


Fig 1 Roll bond evaporator to be used in room air conditioner, showing the path of refrigerant (a) Roll bond panel as evaporator (b) Flow of refrigerant through the roll bond evaporator at section A-A

Thus by applying the coating in a serpentine pattern, it is possible to create a serpentine shaped un-welded region within this welded part. By subsequently applying hydraulic pressure to this un-welded region, it is possible to inflate the un-welded serpentine region to form a serpentine passage through the plate. Thus a plate with an integral serpentine passage can be created in a very cost effective manner. Except for the passage the evaporator plate is primarily flat. One end of the evaporator plate is connected to the exit of expansion valve and the other end to the compressor inlet. The refrigerant passes through the channel and produces the desired refrigeration effect.

II. BACKGROUND

A lot of work has been done earlier on suitability of roll bond evaporator as a heat exchanger device. Numerical models were developed and simulation is carried out. Different manufacturing methods of roll bond evaporator were explored.

Siviero, Roberto [2], in their invention, used a roll bond evaporator for use in refrigerator appliance, in a domestic refrigerator. They have stated that the roll bond technique makes the manufacture of refrigerant circuit simple. Even though there might be some short comings in this method, a skilled art makes the roll bond evaporator to be more suitable for the appliance.

A.G. Janos[3], in his patent presented that the evaporator structure which is of roll bonded type is suitable for general refrigeration application. He has provided a method of manufacturing a roll bond evaporator having a heater wire, which forms an integral part of it. This helps in defrosting.

Fieramonte, Luigi [4], in their patent experimentally found out that the performance of a refrigerator container increases drastically with the use of roll bond evaporator. They conducted experiments on using different materials of different thickness for manufacture of roll bond evaporator and found an optimum solution to increase the performance of refrigerator container.

Anthony J. Cesaroni, Clarence W. Fulton [5], in their patent used a roll bonded metal sheets for making a non planar article. They have demonstrated that this article can be used for automotive heat shield which protects the occupants of any automobile from excessive heat developed by components of exhaust system.

Chandrakant patel [6], in his invention developed a cooling apparatus for a computer sub system. The panel gave maximum cooling when it was configured by a roll bond panel.

Diego Castanon Seoane [7], while developing an atmospheric water generator, which includes a refrigeration system proved that the total system gives an optimum performance, if a roll bond evaporator is used for the refrigeration system.

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Stephen R. Callender [8] had a very interesting observation. He noticed that his family dog always preferred to lie on cool surfaces, like ceramic tiles. In his effort to give comfort to his dog he manufactured a cool surface for the dog to lie on. He observed that the cooling is uniform when the plate is manufactured by roll bonding technique.

JB Thomas [9] has given a detailed account on the method of making evaporators for refrigerators and similar devices. He has further stressed on annealing process so as to give high strength to the panel.

Yilmaz, Turan [10], in their patent gave a different method of production of plate tube type of evaporator. They claimed that the evaporator produced by this process has high heat conductivity

DE IZPARILNIKI [11], in their specification catalogue gave different varieties of roll bond evaporators which fit for different refrigerating systems. The specifications are with respect to the materials used, type of cross section, thickness etc.

Wei Yang and Jyhwen Wang [12], in their study have found that diffusion process which is a primary mechanism for roll bonding of metals sheets will be more compact if it is done by warm rolling process.

Christian J.L Hermes, Claudio Melo, Cezar O.R. Negrao [13], have studied the importance of using a roll bond evaporator in refrigerating system. In their journal paper, they have developed a numerical simulation model for plate type roll bond evaporators. They have validated their results with experimental data.

A. Wintry, MH Al-Hager, Ali A. Bondok [14] in their Journal paper have done CFD analysis of fluid flow and heat transfer in a Roll bonded Plate type radiator made from Aluminum. They have concluded that this method gives higher heat transfer, Low size of radiator and cheaper manufacturing.

Cezar O.R. Regarao, Raul H, Ertal [15], while conducting experiments on domestic refrigerator have developed a Semi Empirical model for steady state simulation of domestic refrigerator. They claimed that this method is simple to evaluate performance of the whole system.

III. REFRIGERANT SIDE (INSIDE) HEAT TRANSFER COEFFICIENT

The heat transfer in any application can be reduced into a simple equation

$$q = U A \Delta t_m$$

Where q is the rate of the rate of heat transfer, U is overall heat transfer coefficient, A is Area of heat transfer and Δt_m is temperature difference (either mean temperature difference, or logarithmic mean temperature difference). The overall heat transfer coefficient can be based on either inside or outside diameter of the roll bond evaporator. In general the overall heat transfer coefficient is given by the relation

$$\frac{1}{U_i A_i} = \frac{1}{U_o A_o} = \frac{1}{\{h.A_f.\eta_f\}_o} + \frac{\Delta x}{k_w A_w} + \frac{1}{\{h.A_f.\eta_f\}_i}$$

Where A is Area of the roll bond evaporator, h is convective heat transfer coefficient, Δx is wall thickness, K_w is thermal conductivity of wall, and η represents efficiency of fin. The subscripts i and o represents inside and outside of the roll bond evaporator.

Evaluation of the inside heat transfer coefficient (refrigerant side) can be done either by single- phase heat transfer analysis or by two phase analysis. But in an evaporator, the refrigerant is predominantly in two phase region. Many correlations are available for the analysis. Dittus- Boelter correlation, Petukhov and Popov correlation, Shah's correlation, Bio – Pierre correlation [1], Chato and Wattleet correlation can be used. But the most important relation for refrigerant side heat transfer coefficient is given in ASHRAE Handbook, Fundamentals volume - 7

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$$\frac{h D}{k} = C_1 \left\{ \left\{ \frac{G D}{\mu} \right\}^2 \frac{J \Delta x h_{fg}}{L g} \right\}^n \dots\dots\dots \text{ {Equation 1} }$$

h is inside heat transfer coefficient, D is inside diameter of the roll bond evaporator, k is thermal conductivity of the refrigerant in liquid phase, C₁ is a constant = 9 x 10⁻⁴ if quality of refrigerant leaving the roll bond evaporator is less than 0.9 and 8.2 x 10⁻³ if quality of refrigerant is greater than or equal to 1. G is mass velocity of refrigerant through evaporator in kg sec⁻¹ m². μ is dynamic viscosity of the refrigerant, J is Joule equivalent, Δ x is change in quality of the refrigerant, h_{fg} is latent heat of vaporisation and L is length of the tube and n is a constant = 0.5 when quality of refrigerant is less than 0.9 and is equal to 0.4 when the quality is greater than or equal to 1. The above equation is solved in SI system of units.

The design is carried out for 1 ½ TR (Ton of Refrigeration) capacity room air conditioner. The refrigerant used in the room air conditioner is R -22 (Mono-Chloro Di-Fluro methane – CHClF₂). The following assumptions are made to carry out the design.

- i. The refrigerant is dry and saturated when it leaves the roll bond evaporator
- ii. There is no under cooling (sub cooling) of refrigerant in condenser.

Design conditions:

Capacity of room air conditioner	–	1 ½ TR
Pressure in Condenser	–	19.423 bar (282 PSI)
Condensing Temperature	–	50 ° C
Pressure in Evaporator	–	5.8378 bar (87.3 PSI)
Temperature in Evaporator	–	5 ° C

The properties of the refrigerant R-22 are taken from ASHRAE. With the above data, the enthalpy of the refrigerant at the entry of compressor (h₁) is 407.45 KJ/Kg and at the entry of evaporator (h₄) is 262.27 KJ/Kg.

Mass flow rate :

The mass flow rate of the refrigerant is evaluated as

$$m \times (h_1 - h_4) = 1.5 \times (210/60)$$

Mass flow rate of refrigerant will be, m = 0.03616 Kg/sec

Quality of refrigerant at the inlet of evaporator:

The expansion process in capillary tube (expansion valve) is isenthalpic process. Equating the enthalpy at inlet and exit of capillary tube

$$h_{f, \text{ at inlet}} = [h_f + x h_{fg}] \text{ at exit}$$

From refrigerant properties h_{f, at inlet} = 263.264 K J/Kg and at exit, h_f = 205.899 KJ/kg , h_{fg} = 201.244 KJ/Kg
 Substituting these values, the quality of refrigerant at the exit of capillary tube, i.e at the inlet of evaporator is 0.285 i.e 28.5 %

Commercially available roll bond evaporators are have outside diameter of 1/4, 3/8, 1/2, 5/8, 1, 1 ¼, 1 ½ inches with lengths 6, 8, 10, 12 , 16 feet , with thickness 14 BWG (Brimingham wire gauge). For the present design the roll bond evaporator having 3/8 inch outside diameter with a length of 6 m is considered. As the tube is of 14 BWG, the inside

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diameter of the roll bond evaporator d_i will be 5.325 mm. The other refrigerant properties like thermal conductivity, dynamic viscosity are taken from ASHRAE refrigerant tables. Now the inside heat transfer coefficient (refrigerant side heat transfer coefficient) of the roll bond evaporator is evaluated from equation 1. The value of heat transfer coefficient, h_i , so obtained was found to be $816.62 \frac{W}{m^2 K}$

The above calculations were repeated fixing diameter of the roll bond evaporator and varying the lengths of the roll bond evaporator. Inside heat transfer coefficient was calculated. The results so obtained are represented graphically in Fig 2.

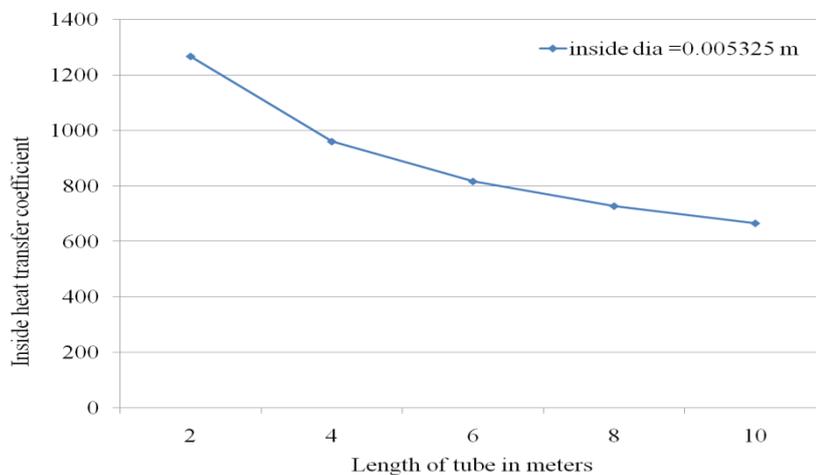


Fig 2. Variation of Inside heat transfer coefficient with length of the roll bond evaporator keeping inside diameter of the tube fixed

The calculations were repeated fixing the length of roll bond evaporator as 6 m, varying the inside diameter of the roll bond evaporator. Inside heat transfer coefficient was calculated. The results so obtained are represented graphically in Fig 3.

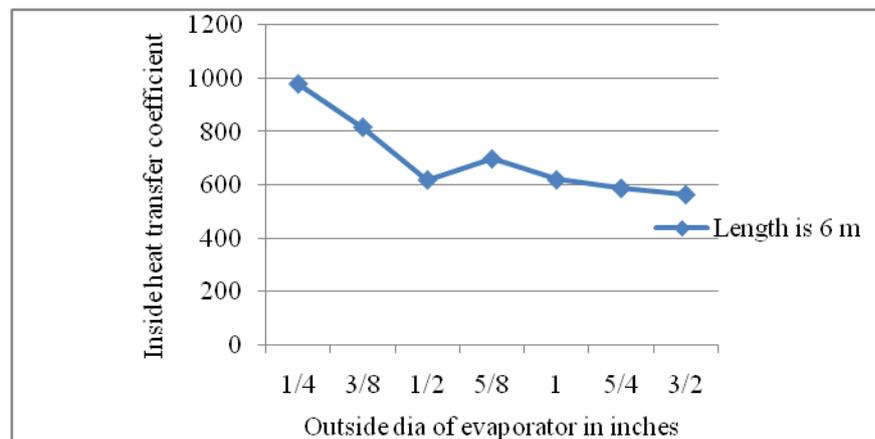


Fig 3. Variation of Inside heat transfer coefficient with outside diameter of the roll bond evaporator keeping length of the evaporator fixed

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IV. CONCLUSIONS

For the above design conditions, i.e 1 ½ TR room air conditioner, a roll bond evaporator has been designed. The inside heat transfer coefficient (refrigerant side) is found to be $816.62 \frac{W}{m^2 K}$. Further, the design has been extended by varying the length of the roll bond evaporator, fixing its diameter and also by varying diameter and fixing the length. It can be concluded from the two graphs that with the increase in length of the evaporator, the inside heat transfer coefficient decreases. Further with increase in outside diameter and hence inside diameter, the inside heat transfer coefficient decreases. The graphs suggests that the roll bond evaporators of outside diameter $\frac{3}{8}$, $\frac{1}{2}$, $\frac{5}{8}$ inches provide optimum performance. As this roll bond evaporator is to be used in room air conditioner, a length of 4m or 6m is preferred.

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