Modeling and Control of Liquid Level Non-linear Interacting and Non-interacting System

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ABSTRACT: Non-linear process control is a difficult problems in process industries. Conical tank level control is one among them. Real processes often exhibits nonlinear behavior, time variance and delays between inputs and outputs. Conical tanks are widely used in many industries due to its shape which provides easy discharge of water when compared to other tanks. Moreover, liquid level control of a conical tank is still challenging for typical process control because of its nonlinearities by a reason of constantly changing cross section area. In this paper the mathematical modeling of three tank conical interacting and non-interacting system is designed by Wiener model PI controller(WMPI) where the tuning rules based on Chidambaram method and the performance criteria are related with Internal mode controller(IMC). Also in this paper we analyze dynamic behavior among interacting and non-interacting system.

KEYWORDS: Non-linear process, WMPI, IMC, Chidambaram tuning rule.

I. INTRODUCTION

Conical tank control of industrial process is a challenging task for numerous bases due to its nonlinearity. The control of liquid level in conical tank is a major trouble in industrial process. A level is far above the surface may possibly disturb process reaction equilibria make happen spoil to equipment. If the height is near to the surface it may perhaps bad result for the series operation. So liquid level control in process industries is significant and general task. Conventional controllers are broadly use in industries since they are trouble free, robust, and well known to the field operator. Practical system are not precisely linear but mat be represented as linearized models around a nominal Operating point, the controller parameters tuned at that point may not reflect the real time system characteristics due to variations in process parameters. For controlling the liquid level in conical tank we make use of Wiener model PI controller(WMPI) where the tuning rules based on Chidambaram method and the results are compared with internal model controller (IMC).In this task the process model is carry out trial and determined by using system identification method. The method adopted here for system identification is step test and is done in real time with Labview using NI DAQ.

II.PROCESS BLOCK DIAGRAM

A real time experimental setup for extremely non-linear conical tank is constructed. The process control system is interfaced with labview using PCI 6221 DAQ module to the personal computer. The block diagram for this system is shown in Figure 1, it consists of a labview based controller, driver circuit used to operate the solenoid valve, nonlinear conical tank, capacitance based level sensor, signal conditioning unit.
The control parameter prefers here is the level. Capacitance based level transmitter arrangement senses the level from the process and converts into electrical signal. Then the corresponding electrical signal is fed to the current to voltage converter which in turn produces proportional voltage signal to the computer.

The experimental setup shows the closed loop system which maintains water level in a conical tank and also perform the non-interacting & interacting. The actual tank water level sensed by the level transmitter is feedback to the level controller & compared with a desired level to produce the required control action that will position the level control as needed to maintain desired level. Now the controller decides the control action & it is given to the voltage to current converter. The FCE is now controlled by the resulting pneumatic signal. This in turn control the inflow to the conical tank & the level is also controlled in both non-interacting & interacting system.

The Tank Specifications are as follows:
- Height: 40 cm
- Volume: 11.39 litres
- Bottom diameter: 10 cm
- Top diameter: 25 cm
- Angle: 10 deg
- Material: Stainless Steel

IV. MATHEMATICAL MODELING

A. Mathematical Modeling of Two Conical Tanks of Non-Interacting System

System is said to be non-interacting the dynamic behaviour of the first system will affect the dynamic behaviour of the second system while the dynamic behaviour of the second system does not affect the first system.

Let us define,
- $H_1 =$ height of the conical tank 1 cm
- $H_2 =$ height of the conical tank 2 cm
- $V =$ total volume of the conical tank
- $q_{in}(s) =$ volumetric flow rate of the inlet stream (lph)
q_1(s)\text{volumetric flow rate of the outlet stream (lph)}
\text{R}_1=\text{Restriction element}

\text{H=Maximum height of the conical tank}

\text{According to law of conservation of mass,}
\text{Accumulation of mass within a system} = \text{Flow of mass into the system} - \text{Flow of mass out to the system}

\frac{\text{d}h_1}{\text{d}t} = q_{in} - q_1

(1)

For laminar flow,
q_1 = \frac{h_1}{R_1}

(2)

Sub (2) in (1)
\frac{\text{d}h_1}{\text{d}t} = \frac{h_1}{R_1}

(3)

On taking Laplace transform
V_1(s) * \frac{h_1(s)}{s} = q_{in}(s) - \frac{h_1(s)}{R_1}

(4)

Similarly for tank-2
H_2(s) = \frac{K_p}{\tau_2s + 1}

q_1(s) = \frac{k_p}{\tau_2s + 1}

q_0(s) = \frac{k_p}{\tau_2s + 1}

(5)

(6)
For a combined tank with $q_{in}(s)$ and $q_{out}(s)$ as inflow and outflow parameters, then the overall transfer function is given by

$$
\frac{q_{in}(s)}{q_{out}(s)} = \frac{1}{(\tau_1 s + 1)(\tau_2 s + 1)}
$$

(7)

For a real-time process, the transfer function of a non-interacting conical tank system is given by,

$$
\frac{q_{in}(s)}{q_{out}(s)} = \frac{378e^{-40s}}{5751.71s^2 + 341.28s + 378}
$$

(8)

### B. Mathematical Modeling of Two Conical Tanks of Interacting System

System is said to be interacting then the dynamic behavior of the first system will affect the dynamic behavior of the second system while the dynamics of the second system will affect the dynamics of the first system.

For tank 1,

$$
v_1 \frac{dh_1}{dt} = q_{in} - q_1
$$

$$
q_1 = \frac{h_1 - h_2}{R_1}
$$

$$
v_1 \frac{dh_1}{dt} = q_{in} - \frac{h_1 - h_2}{R_1}
$$

(9)

For tank 2,

$$
v_2 \frac{dh_2}{dt} = q_1 - q_0
$$

Let $q_0 = \frac{h_1}{R_2}$

$$
v_2 \frac{dh_2}{dt} = \frac{h_1 - h_2}{R_1} - \frac{h_2}{R_2}
$$

(10)

On solving the above equation we get,
For a real time process the overall system transfer function of interacting conical tank system is given by

\[
\begin{align*}
\frac{h_2(s)}{q_{in}(s)} &= \frac{R_2}{(\tau_1 \tau_2 s^2 + (\tau_1 + \tau_2 + \nu_1 \tau_2) s + 1)R_2} \\
\frac{h_1(s)}{q_{in}(s)} &= \frac{(R_1 \tau_2 s + R_1 s + R_2)}{s^2 + (\tau_1 + \tau_2 + \nu_1 \tau_2) s + 1} \\
\frac{q_o(s)}{q_{in}(s)} &= \frac{1}{(\tau_1 \tau_2 s^3) + (\tau_1 + \tau_2 + V_1 \tau_2) s + 1} \\
\end{align*}
\]

For a real time process the overall system transfer function of interacting conical tank system is given by

\[
G(s) = \frac{529e^{-40s}}{3010.08s^2 + 341.28s + 529}
\]

V. TECHNIQUE FOR CONTROLLER DESIGN

A. COHEN COON METHOD

For a non-linear system the output to be settled region by region for finding that we divide our measurements in three sections like 0 to 12 cm, 12 to 24 cm, and 24 to 36 cm.

We obtain the transfer function from the experimental data.

From this transfer function obtain kc, ti, td by using cohen coon method and simulated this value using matlab for the output response.

![Figure 5 open loop response of the process](image)

With respect to the order of the system the shape of the system will varies. Whatever may be the order we are approximating first order with dead zone.

1. Bring the system or a process to a steady state value.
2. Give a small step change to the input. Sketch the response.
3. The point at which the response starts increase vertically is known as point of inflection.
4. Draw a tangent on the point of inflection.
5. The point at which the tangent meets the time X-axis is dead time.
6. Draw a slope on the tangent and let it be slope.
Ziegler Nichols is a method of controller setting assignment that has come to be associated with their name. This technique, also called the ultimate cycle method, is based on adjusting a closed loop until steady oscillations occur. Controller settings are then based on the conditions that generate the cycling. The PI parameters are calculated as: 

\[ K_c = \frac{0.9 \tau_i}{\tau_d} \]  \( \tau_i = 3.33 \tau_c \). The general drawback is that the resulting closed loop system is often more oscillatory than desirable.

C. Internal Model Controller

The controller is designed to provide nominal performance, and a non-linear filter is added to make the controller implementable and to account for plant/model mismatch. An important advantage of the new approach is that the assumption of full-state feedback inherent in most input-output linearization schemes is eliminated. However, the proposed IMC strategy is restricted to open-loop stable systems with stable inverses. Under mild assumptions, the closed-loop system possesses the same stability, perfect control, and zero offset properties as linear IMC. The PI parameters are calculated as:

\[ K_c = \frac{\tau_i + \tau_d}{\tau_i \tau_d} \]  \[ \tau_i = \frac{\tau_i}{\tau_i + \tau_d} \].

<table>
<thead>
<tr>
<th>System</th>
<th>cases</th>
<th>kc</th>
<th>( \tau_i )</th>
<th>( \tau_d )</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0 - 12</td>
<td>0.07</td>
<td>81.68</td>
<td>40</td>
</tr>
<tr>
<td></td>
<td>12 - 24</td>
<td>0.02</td>
<td>110.7</td>
<td>50</td>
</tr>
<tr>
<td></td>
<td>24 - 36</td>
<td>0.01</td>
<td>66.67</td>
<td>20</td>
</tr>
<tr>
<td>Interacting</td>
<td>0 - 12</td>
<td>0.06</td>
<td>75.46</td>
<td>30</td>
</tr>
<tr>
<td></td>
<td>12 - 24</td>
<td>0.02</td>
<td>90.59</td>
<td>40</td>
</tr>
<tr>
<td></td>
<td>24 - 36</td>
<td>0.01</td>
<td>91.03</td>
<td>40</td>
</tr>
</tbody>
</table>

Table 2 performance of IMC based tuning

<table>
<thead>
<tr>
<th>System</th>
<th>cases</th>
<th>kc</th>
<th>( \tau_i )</th>
<th>( \tau_d )</th>
<th>ISE</th>
<th>IAE</th>
<th>ITAE</th>
</tr>
</thead>
<tbody>
<tr>
<td>Non-Interacting</td>
<td>0-12</td>
<td>0.09</td>
<td>151.68</td>
<td>40</td>
<td>800</td>
<td>80</td>
<td>320</td>
</tr>
<tr>
<td></td>
<td>12-24</td>
<td>0.06</td>
<td>366.56</td>
<td>30</td>
<td>600</td>
<td>60</td>
<td>18</td>
</tr>
<tr>
<td></td>
<td>24-36</td>
<td>0.03</td>
<td>227.52</td>
<td>20</td>
<td>700</td>
<td>70</td>
<td>245</td>
</tr>
<tr>
<td>Interacting</td>
<td>0-12</td>
<td>0.05</td>
<td>341.28</td>
<td>30</td>
<td>800</td>
<td>80</td>
<td>320</td>
</tr>
<tr>
<td></td>
<td>12-24</td>
<td>0.03</td>
<td>379.2</td>
<td>40</td>
<td>300</td>
<td>30</td>
<td>45</td>
</tr>
<tr>
<td></td>
<td>24-36</td>
<td>0.02</td>
<td>404.28</td>
<td>40</td>
<td>400</td>
<td>40</td>
<td>80</td>
</tr>
</tbody>
</table>
C. PADMASREE-SRINIVAS-CHIDAMBARAM TECHNIQUE (PSCT)

The performance specification for stable system cannot be met for the unstable system. Chidambaram have used tuning parameter. The performance of the controller designed by the method significantly better than that of pole placement method. Later Chidambaram and padmasree have extended the method to integrating system with dead time, and the performance of the controller designed is significantly better than that of the optimization method. The PI parameters are calculated as: $k_c*\frac{k_p}{(\tau/\tau_d)+0.5}$;

$\tau_i=\tau+0.5\tau_d$.

Table 3 performance of PSCTR

<table>
<thead>
<tr>
<th>system</th>
<th>cases</th>
<th>kc</th>
<th>td</th>
<th>ISE</th>
<th>IAE</th>
<th>ITAE</th>
</tr>
</thead>
<tbody>
<tr>
<td>Non-Interacting</td>
<td>0-12</td>
<td>0.06</td>
<td>40</td>
<td>200</td>
<td>20</td>
<td>20</td>
</tr>
<tr>
<td></td>
<td>12-24</td>
<td>0.03</td>
<td>30</td>
<td>300</td>
<td>30</td>
<td>45</td>
</tr>
<tr>
<td></td>
<td>24-36</td>
<td>0.02</td>
<td>20</td>
<td>400</td>
<td>40</td>
<td>80</td>
</tr>
<tr>
<td>Interacting</td>
<td>0-12</td>
<td>0.05</td>
<td>30</td>
<td>400</td>
<td>40</td>
<td>80</td>
</tr>
<tr>
<td></td>
<td>12-24</td>
<td>0.02</td>
<td>40</td>
<td>700</td>
<td>70</td>
<td>245</td>
</tr>
<tr>
<td></td>
<td>24-36</td>
<td>0.01</td>
<td>40</td>
<td>1500</td>
<td>150</td>
<td>1125</td>
</tr>
</tbody>
</table>
The Table - 4 represent the calculation of error for both Non-Interacting & Interacting systems by using IMC & CHIDAMBARAM techniques. By comparing these two techniques the error was minimized in Chidambaram technique. So that wiener model PI controller was designed using Chidambaram technique.
VI. WIENER MODEL BASED PI CONTROLLER

The aim of this study was the development and real-time implementation of a Wiener model-based PI controller (WMPIC) for a conical tank level process. The conical tank level process exhibits severe static non-linear behaviour and dynamic characteristics. Here, a WMPIC structure was developed by the way of compensating the process static non-linearity. Tuning rules suggested by Padmasree-Srinivas-Chidambaram and internal model controller were considered here for designing the controller. The real-time implementation results of Wiener model based PI controller were designed. The performance of this controller was analyzed in terms of Integral Square Error (ISE), Integral Absolute Error (IAE), Integral Time Absolute Error (ITAE).

A. PROCEDURE FOR DESIGNING WMPIC:

- From the tentative information, worst case of model parameters is selected. Larger process gain, larger delay, and smaller time constant of the process.
- PI controller settings have been evaluated based on the above selected model parameters using PSCTR (Padmasree-Srinivas-Chidambaram tuning rules) and IMC (internal model controller).
- Using the values obtained in step no.: (1 & 2) developed a Wiener model based PI controller.

Table 5 Performance of Wiener model PI controller

<table>
<thead>
<tr>
<th>System</th>
<th>Ke</th>
<th>τi</th>
<th>τd</th>
<th>ISE</th>
<th>IAE</th>
<th>ITAE</th>
</tr>
</thead>
<tbody>
<tr>
<td>Non-Interacting</td>
<td>0.0114</td>
<td>151.68</td>
<td>40</td>
<td>300</td>
<td>30</td>
<td>45</td>
</tr>
<tr>
<td>Interacting</td>
<td>0.0171</td>
<td>341.28</td>
<td>40</td>
<td>400</td>
<td>40</td>
<td>80</td>
</tr>
</tbody>
</table>

VII. SIMULATION RESULTS

The simulation and real-time responses for Wiener model PI control scheme for non-interacting non-linear system and interacting non-linear system were experienced at different operating points. The simulation was passed out using MATLAB and the real-time control of both interacting & non-interacting was done with LabVIEW. Fig. 18 and Fig. 19 show the simulated response of conical tank interacting system and conical tank non-interacting system was done with various operating point and Fig. 20 and Fig. 21 show the real-time control of both interacting & non-interacting with Wiener model PI controller.
Figure 12 Wiener Non-Interacting

Figure 13 Wiener Interacting

Figure 14 Block diagram

Figure 15 Front panel
VIII CONCLUSION AND FUTURE WORK

The wiener model PI controller is designed and applied to both non-interacting & interacting system for level control. The wiener model PI controller parameters are tuned for several height of tank and then it is simulated under parameter changes. Control of liquid level in the both non-interacting & interacting system process is a difficult task because of its non-linear behaviour. By proper wiener model PI controller tuning, level control all the categories is first carried out in matlab and then analyzed in real time using labview. The future work can be extended for controlling of both non-interacting & interacting using artificial intelligence.

REFERENCES


BIOGRAPHY

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