

Performance Analysis of Three Phase Matrix Converter for Induction Motor

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ABSTRACT— The motivation of this project is to produce three phase voltage with variable frequency and amplitude. This is achieved with the help of matrix converter, which is single stage AC/AC converter. It has more characteristics like sinusoidal input and output currents, voltage, unity displacement factor and limited frequency changer. The various modulation algorithms are used to control matrix converter. Most ideology behind the modulation algorithm is to get output voltages from input desired frequency and amplitude. The modulation algorithm can be applied to both direct and indirect matrix converter. The induction motor fed by three phase direct matrix converter which makes directly AC-AC power conversion is modelled using Space Vector Modulation technique for direct matrix converter in Matlab& Simulink. In this method, gate drive signals for the nine bidirectional switches are calculated to generate variable frequency and amplitude of sinusoidal output voltage from fixed frequency and amplitude of input voltage. This model provides the output upto 86.6% of input voltage and unity power factor. And also it reduces the effective switching frequency in each cycle and reducing the switching losses.

KEY WORDS: Matrix converter, Space Vector Modulation.

I. INTRODUCTION

Three phase matrix converter is an AC-AC power converter with nine bidirectional switches. Which are arranged as 3×3 matrix and with any output phase can be connected to any input phase. Some of the advantages over this converter are providing bidirectional power flow, absence of DC link capacitor, sinusoidal input and output current with adjustable displacement angle.

Various modulation strategy for matrix converter has been investigated due to harmonic spectrum, total harmonic distortion (THD), complexity of implementation and switching play an important roles. A complete

mathematical analysis of the power circuit along with duty cycle calculation is proposed for both low voltage transfer ratio and high voltage transfer ratio. The basic matrix converter is shown in below fig.1.

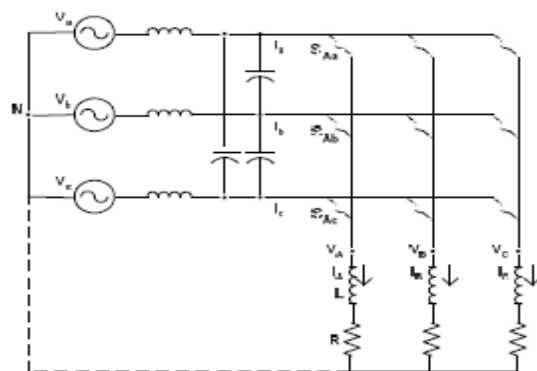


Fig. 1 Three phase matrix converter

Analysis and mathematical modeling of space vector modulated direct controlled matrix converter IEEE (2010) presented a paper about mathematical model for a space vector modulated (SVM) direct controlled matrix converter. Modelling stability analysis and control of a direct AC/AC matrix converter based systems MelakuMihretIEEE (2011) presented about direct and indirect space vector modulation using matrix converter switching configuration .To design a input filter to maintain a harmonics balance technique.

An effective direct SVM method for matrix converter operating with low voltage transfer ratio, Hong Hee lee IEEE (2012) deals with the Common mode voltage using the direct space vector modulation for power factor compensation. Analysis and mathematical modeling for Space Vector modulated direct controlled matrix converter RuzlainiGhoni IEEE(2013) presented a paper about mathematical model for a space vector modulated (SVM)

direct controlled matrix converter. The duty cycles of the switches are modeled using space vector modulation for voltage transfer ratios about 0.5 to 0.866. The matrix converter simulations are loaded by passive RL load and active induction motor are performed.

In this paper design a matrix converter which is a AC-AC power converter which is composed of an array of mxn bidirectionalsemiconductor switches, connecting each phase of the input to each phase of the output using venturini and space vector method which provides sinusoidal input and output waveforms, with minimal higher order harmonics and no sub harmonics. The output is tested for different load condition.

II. SPACE VECTOR MODULATION

The space vector algorithm is based on the representation of the three phase input current and three phase output line voltages on the space vector plane. Space Vector modulation is a special switching sequence which is based on upper switches of a three phase direct matrix converter. SVM which treats a sinusoidal voltage as a phasor or amplitude and it rotates at a constant frequency ω. The amplitude vector which is represented as d-q plane and it denotes the real and imaginary axes.

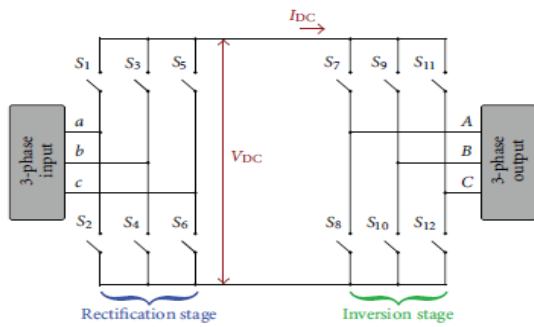


Fig. 2 Three phase Matrix converter

For any combination output voltage and input current sectors, the four combinations can be identified, which reduce output voltage and input current vectors. Four switching patterns are analyzed and simulated for direct space vector modulation they are asymmetrical single sided, which uses only one of the three zero vectors.

The switching combinations can be classified into three groups they are synchronously rotating vectors, stationary vectors and zero vectors. Matrix converter connects load directly to the voltage source by using nine bidirectional switches, the input phases should not be short circuited due to inductive nature of the load, the output phases should not be kept open. If the switching function of a switch, s_{ij} in equation (1)

$$s_{ij} = \begin{cases} 1 & s_{ij} \text{ open} \\ 2 & s_{ij} \text{ close} \end{cases} \quad i \in \{u, v, w\}, j \in \{a, b, c\} \quad (1)$$

For a balanced three phase sinusoidal system the instaneous voltage may be expressed in equation (1)

$$\begin{bmatrix} v_u(t) \\ v_v(t) \\ v_w(t) \end{bmatrix} = \begin{bmatrix} \cos w_0(120^\circ) \\ \cos(w_0 t - 120^\circ) \\ \cos(w_0 t - 240^\circ) \end{bmatrix} \quad (2)$$

III CONTROL ALGORITHM

The transfer function approach is applied for both Voltage Source Inverter (VSI) and Voltage Source Rectifier (VSR).

A. Space vector modulation for rectifier stage

The rectifier part of equivalent circuit for Current Source Rectifier (CSR) with averaged value of I_{DC} may be expressed in equation (2)

$$I_{DC} = \frac{\sqrt{3}}{2} I_{out} \cdot m_v \cdot \cos(\theta_{out}) \quad (3)$$

I_{out} is a peak value current, θ_{out} is a output load displacement angle, $m_v = V_{out}/V_{DC}$. The space vector of the desired output can be approximated by two adjacent. The duty cycle of the VSR are calculated as

$$d_{\alpha i} = m_i \cdot \sin\left(\frac{\pi}{3} - \theta_i\right) \quad (4)$$

$$d_{\beta i} = m_i \cdot \sin\theta_i \quad (5)$$

$$d_{\theta i} = 1 - d_{\alpha i} - d_{\beta i} \quad (6)$$

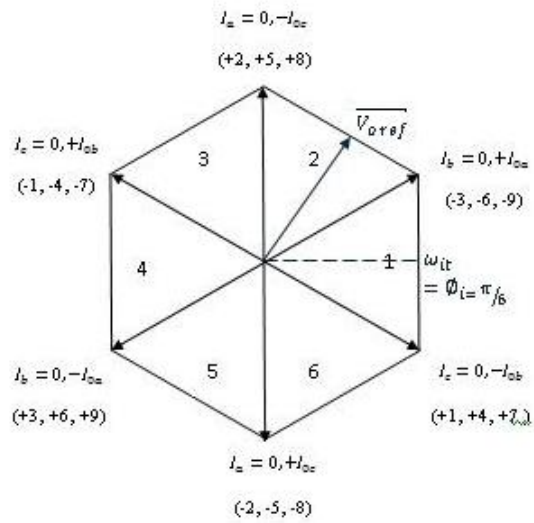


Fig. 3 Input Current Vector

The Rectifier Input Current vector diagram is shown in Fig 3. The nine Rectifier switches have nine permitted combination to avoid an open circuit in DC link.

$$\begin{bmatrix} \vec{i}_a \\ \vec{i}_b \\ \vec{i}_c \end{bmatrix} = \begin{bmatrix} d_{\alpha i} + d_{\beta i} \\ -d_{\alpha i} \\ -d_{\beta i} \end{bmatrix} \cdot I_{dc}$$

$$=m_i \cdot \begin{bmatrix} \cos\left(\theta_i - \frac{\pi}{6}\right) \\ -\sin\left(\frac{\pi}{3} - \theta_i\right) \\ -\sin(\theta_i) \end{bmatrix} \cdot I_{dc} \quad (7)$$

The switching cycle within the first vector is given by equation (7).

B. Space vector modulation for inverter stage

The inverter can be assumed as a separate VSI. The switching method is exactly similar to conventional VSI, but owing to its virtual DC link, V_{DC} should be defined in following equation (8) and the output voltage vector is represented in fig 4

$$V_{DC} = \frac{3}{2} V_{in} \cdot m_c \cdot \cos(\theta_{in}) \quad (8)$$

V_{in} is a peak value of input voltage and θ_{in} is an input displacement angle. The VSI switches can assume only six allowed combinations which yield nonzero output voltages. The inverter switches have eight permitted combinations to avoid a short circuit. These combinations include three zero and six non zero input currents.

$$d_{\alpha v} = m_v \cdot \sin\left(\frac{\pi}{3} - \theta_v\right) \quad (9)$$

$$d_{\beta v} = m_v \cdot \sin\theta_v \quad (10)$$

$$d_{\theta v} = 1 - d_{\alpha v} - d_{\beta v} \quad (11)$$

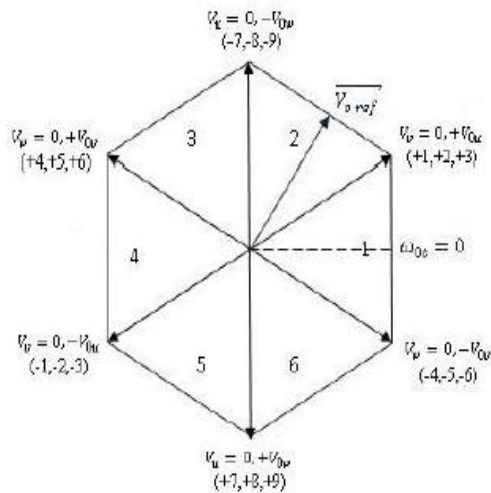


Fig. 4 Output Voltage Vector

The modulation algorithm is derived similar to VSR and VSI except in the opposite direction. Since, both the VSR and VSI hexagons contain six sextants, there are 36 combinations or operating modes. The Table 1 and Table 2 which describes the current and voltage vector.

$$\begin{bmatrix} \vec{i}_a \\ \vec{i}_b \\ \vec{i}_c \end{bmatrix} = \begin{bmatrix} d_{\alpha v} + d_{\beta v} \\ -d_{\alpha v} \\ -d_{\beta v} \end{bmatrix} \cdot V_{dc}$$

$$=m_v \cdot \begin{bmatrix} \cos\left(\theta_v - \frac{\pi}{6}\right) \\ -\sin\left(\frac{\pi}{3} - \theta_v\right) \\ -\sin(\theta_v) \end{bmatrix} \cdot V_{dc} \quad (12)$$

The duty cycle of VSI are calculated in equation (13). 27 valid switch combinations giving the 27 voltage vectors.

Table 1
Current Vector for Rectifier Stage

TYPE	VECTOR	I_{ref}	S_1	S_2	S_3	S_4	S_5	S_6
ACTIVE	I_1	$2/\sqrt{3} I_{DC} < -\pi/6$	1	0	0	1	0	0
ACTIVE	I_2	$2/\sqrt{3} I_{DC} < \pi/6$	1	0	0	0	0	1
ACTIVE	I_3	$2/\sqrt{3} I_{DC} < \pi/2$	0	0	1	0	0	1
ACTIVE	I_4	$2/\sqrt{3} I_{DC} < 5\pi/6$	0	1	1	0	0	0
ACTIVE	I_5	$2/\sqrt{3} I_{DC} < -5\pi/6$	0	1	0	0	1	0
ACTIVE	I_6	$2/\sqrt{3} I_{DC} < \pi/2$	0	0	0	1	1	0
ZERO	I_0	0	1	1	0	0	0	0
ZERO	I_0	0	0	0	1	1	0	0
ZERO	I_0	0	0	0	0	0	1	1

Table 2
Voltage Vector for Inverter stage

TYPE	VECTOR	V_{ref}	S_7	S_8	S_9	S_{10}	S_{11}	S_{12}
ACTIVE	V_1	$2/\sqrt{3} I_{DC} < -\pi/6$	1	0	0	1	0	1
ACTIVE	V_2	$2/\sqrt{3} I_{DC} < \pi/6$	1	0	1	0	0	1
ACTIVE	V_3	$2/\sqrt{3} I_{DC} < \pi/2$	0	0	1	0	0	1
ACTIVE	V_4	$2/\sqrt{3} I_{DC} < 5\pi/6$	0	1	1	0	1	0
ACTIVE	V_5	$2/\sqrt{3} I_{DC} < -5\pi/6$	0	1	0	1	1	0
ACTIVE	V_6	$2/\sqrt{3} I_{DC} < \pi/2$	0	0	0	1	1	0
ZERO	V_0	0	1	0	1	0	1	0
ZERO	V_0	0	0	1	0	1	0	1

IV SIMULINKMODEL

The complete space vector modulation is shown in fig 5. It comprises of Input modulator, Output modulator, Matrix converter modulator and Matrix converter IGBT switches.

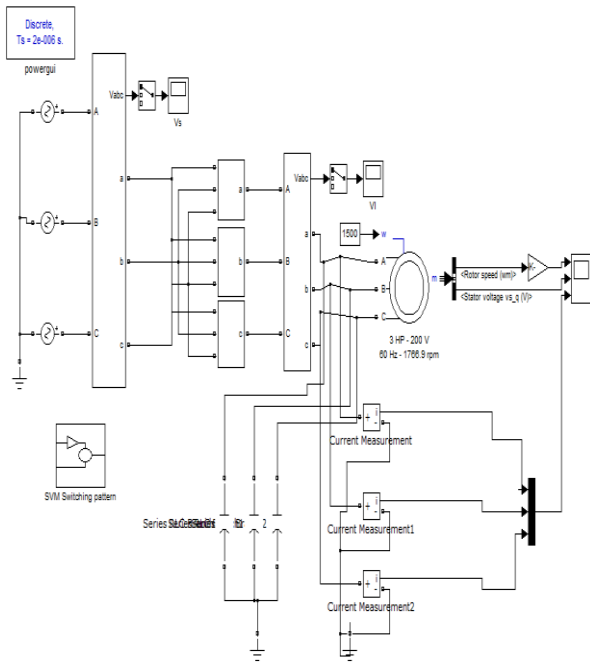


Fig. 5 Space Vector Modulation

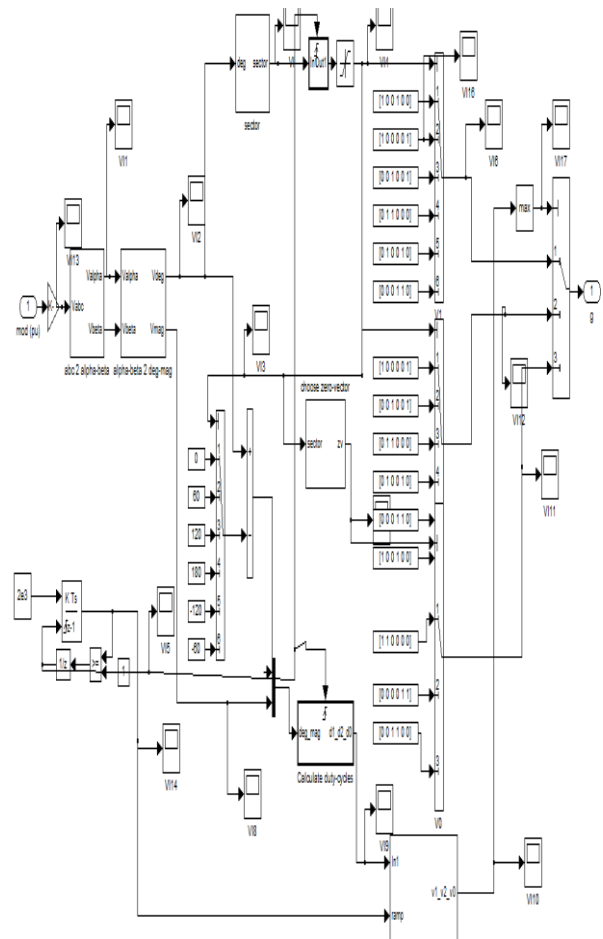


Fig. 7 Input modulation

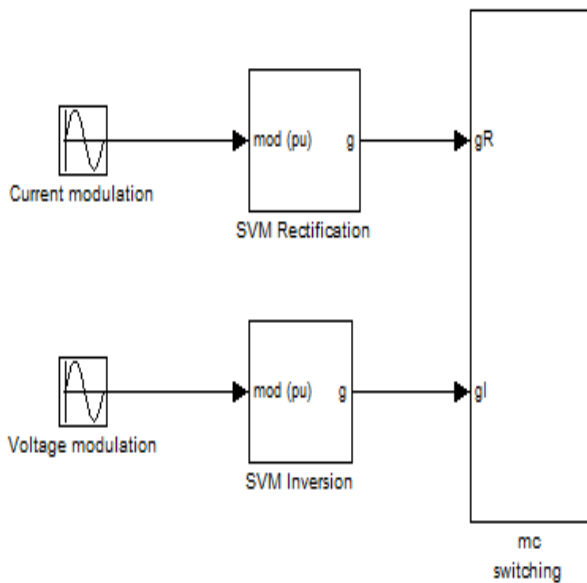


Fig. 6 Simulink model

The Fig 6 which shows the simulation model. Simulation model which consist of current modulation and voltage modulation which is shown in Fig 7 and 8 through which it is connected to SVM rectification and Inversion model.

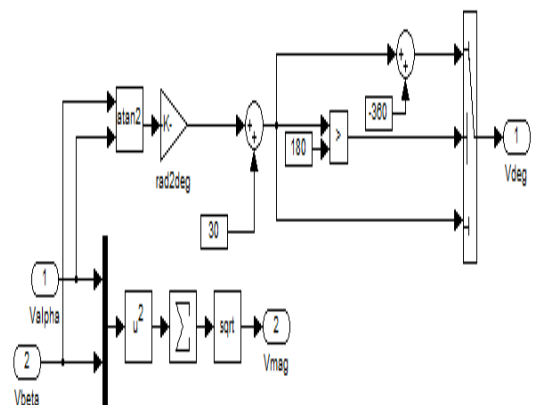


Fig. 8 Formulae for Modulation

V. SIMULATION RESULT

The performance of the direct space vector modulation method is applied to an AC/AC matrix converter. Through matrix converter voltage source is connected to the resistive load. The main circuit is to ideal, and the results are calculated under the conditions of input power supply and output load.

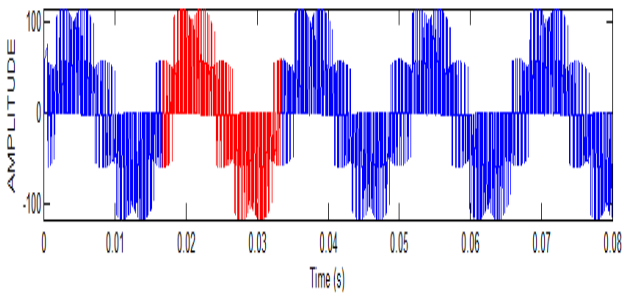


Fig. 9 Output voltage for 50 Hz

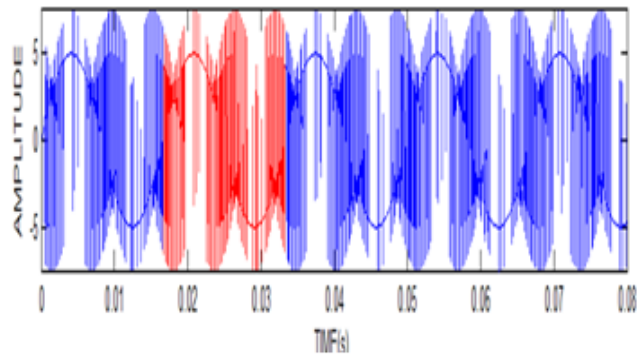


Fig. 10 Output Filter

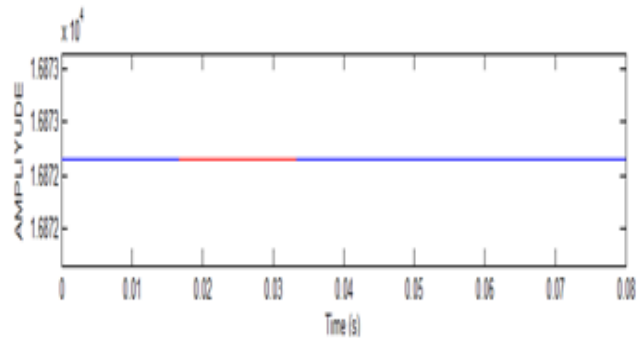


Fig. 11 Rotor Speed

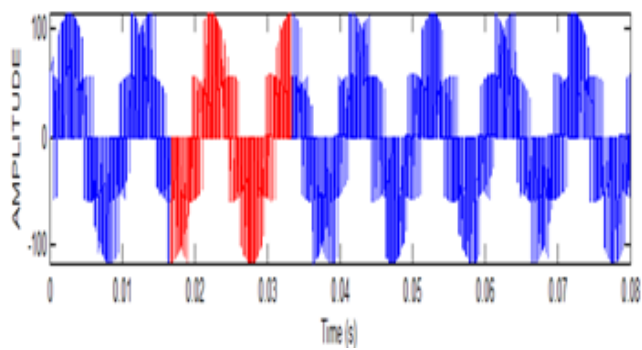


Fig. 12 Output Voltage for 100 Hz

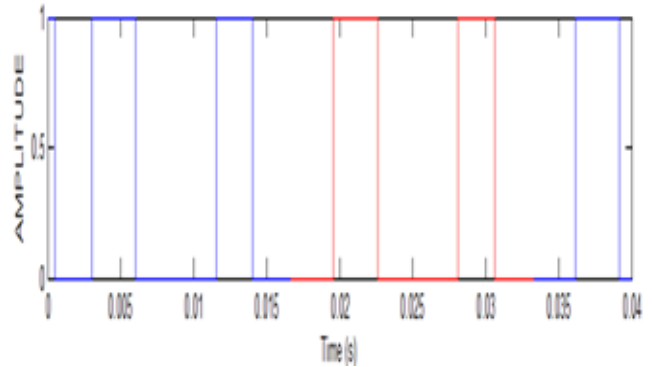


Fig. 13 Pulse Width Modulation.

Furthermore Fig 9 illustrates the Output voltage for 50 Hz, Fig 10 illustrates the Output Filter, Fig 11 illustrates the Rotor speed, Fig 12 illustrates the Output voltage for 100 Hz, and Fig 13 illustrates the Pulse Width Modulation. Through low pass filter higher order harmonics are removed.

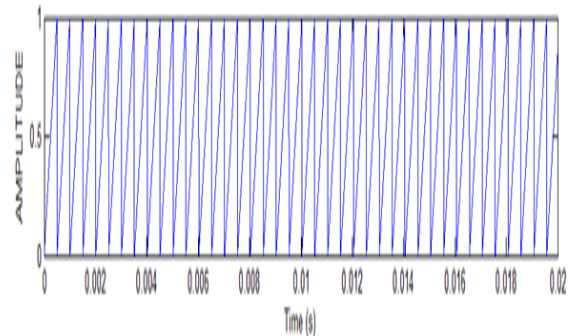


Fig. 14.A Sector Identification

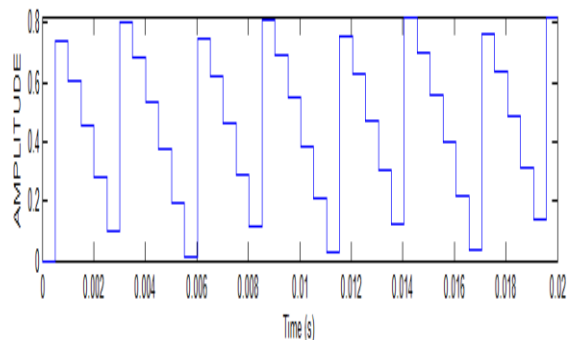


Fig. 14.B Sector Identification

The Simulation result carried out using MATLAB/SIMULINK. It was loaded by three phase induction motor with 3hp, 200V, 60Hz star connected. Fig.14 A&B represents the sector identification and reference angle generation. The angle is generated

from the reference output frequency by integrating. The input and output line voltage with loaded passive load.

VI. CONCLUSION

The simulink model of direct matrix converter for control strategies like SVM technique has been developed and its result are analysed. The significant target to achieving frequency and amplitude has been attaining from input by duty cycle calculation and sequential piecewise sampling. As discussed earlier the direct matrix converter has no efficiency than indirect matrix converter. This constraint has been overcome by the mathematical model that resembles the operation of power conversion stage of matrix converter. This makes the upcoming research on matrix converter is easy and prosperous.

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