



Study of Microstrip Patch Antenna with Complimentary Dual Split Ring Resonator

Prashant R.T,¹ Vani R. M², Hunagund P.V.³

Research Student, Dept. of P G Studies and Research in Applied Electronics, Gulbarga University, Gulbarga,
Karnataka, India¹

Professor & Head, University Science Instrumentation Centre, Gulbarga University, Gulbarga, Karnataka, India²

Professor, Dept. of P G Studies and Research in Applied Electronics, Gulbarga University, Gulbarga, Karnataka, India³

ABSTRACT: In this paper microstrip antenna with Complimentary Dual Split Ring Resonator (CDSRR) is designed using IE3D simulation software and measured practically. The array of 1 x 3 CDSRR is embedded in the ground plane and the study has been made by increasing the number of CDSRRs to 3 x 3 configuration. The measured results shows the antenna with 3 x 3 CDSRRs behind the radiating patch is resonating at two different frequencies i.e., 5.32GHz and 9.45GHz., whereas, antenna without CDSRRs i.e., conventional antenna is resonating at 5.98GHz. The size reduction of 10.86% with return loss (RL) up to -27.33dB ($|S_{11}| < -10\text{dB}$) is achieved. Along with miniaturization the overall bandwidth of 13.85% is achieved. These antennas find application in C and X-bands.

KEYWORDS: microstrip patch antenna; CDSRRs; miniaturization; bandwidth; IE3D

I. INTRODUCTION

Microstrip antennas have unique features and attractive properties such as low profile, light weight, compactness and conformability in structure. With those advantages, the antennas can be easily fabricated and integrated in solid-state devices [1-3]. Microstrip antennas are widely applied in radio frequency devices with single ended signal operation. This has recently been used in microwave design with a combination of metamaterials, either as a cover or a substrate. In modern wireless communication systems, the microstrip patch antennas are commonly used in the wireless devices. Therefore, the miniaturization of the antenna has become an important issue in reducing the volume of entire communication system. V.G. Veselago in 1968 provided a theoretical report on the concept of metamaterial (MTM). These Metamaterials are typically realized artificially as composite structures that are composed of periodic metallic patterns printed on dielectric substrates. Metamaterials have been extensively studied in the recent years, in the framework of microwave applications. Several works have been aimed towards the improvement of the performances of antennas in the microwave range of frequencies [4]. It is noted that some principal properties of waves propagating in materials with negative permittivity and negative permeability are considered [5] and high directivity can be obtained from conventional antenna using Metamaterials.

The Metamaterial would include the SRR and CSRR has a special meaning in the field of microstrip antenna. Split ring resonators (SRR) are an integral component in realizing artificially engineered negative refractive index metamaterials. Their electrical behavior is observed for an axial magnetic field for which these are seldom used in microstrip configuration. On the contrary the complementary split ring resonators (CSRR) are favorable for microstrip application as it responds to axial electric field. This property has been recently harnessed in designing planar microwave components [6-7]. Here in this work the complimentary dual split ring resonator (CDSRR) have been realized on the ground plane of a rectangular microstrip antenna (RMSA) and the corresponding behavior have been studied using method of moment full wave electromagnetic simulation software IE3D™. In IE3D any polygon on the ground is layer treated as a slot [8]. A Dual split ring resonator (DSRR) and its complementary are illustrated in Fig. 2. The complementary is the etched out portion of the DSRRs in the ground plane. In this paper, the miniaturized microstrip patch antenna with CDSRRs is presented.

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 2, Issue 8, August 2014

II. DESIGN OF ANTENNA AND DS-CSRR STRUCTURE

Fig. 1(a) shows the geometry of the proposed conventional microstrip antenna, with a low cost glass epoxy FR4 dielectric material with relative permittivity (ϵ_r) of 4.4 with thickness (h) of 1.6mm is chosen. The conventional MSA is designed for 6 GHz with dimensions L and W radiating part, which is excited by simple 50Ω microstrip feed having dimensions length L_f and width W_f using quarter wave length transformer of dimension length L_t and W_t for their impedance matching. The length L_g and W_g of the ground plane of the antenna is calculated by $L_g=6h+L$ and $W_g=6h+ W$ and all the dimensions are shown in table 1.

The study is carried by etching square CDSRRs in the ground plane as shown in fig. 1(b). Initially the arrays of three CDSRRs are etched from the ground plane with location of $(x, y) = (0, 0)$ mm with spacing between each CDSRRs is 0.8mm which is named as Antenna1. Next another antenna with 2×3 CDSRRs array is introduced with location of $x = 4$ mm and $y= 0$ mm which is named as Antenna2. Finally, the Antenna 3 which is array of 3×3 CDSRRs with locations $x= (-4, 0, 4)$ mm and $y= (0, 0, 0)$ mm with spacing between each CDSRRs is 0.8 mm are etched exactly under the area of radiating patch which is shown in Figure 1(d). By increasing the array of CDSRRs the antenna resonating frequency is shifted towards left and the size of the antenna is virtually reduced with multiple resonating points. So, the final optimized Antenna i.e., Antenna 3 which is resonating at two different frequency points. The parameters of the CDSRR is $S_L = 3.2$ mm, $S_w = 0.2$ mm, $g = 0.2$ mm and $S = 1.6$ mm. Fig. 2 shows the enlarged geometry of CDSRR with variables. Figure 3 is Photographic view of the optimized microstrip patch antenna.

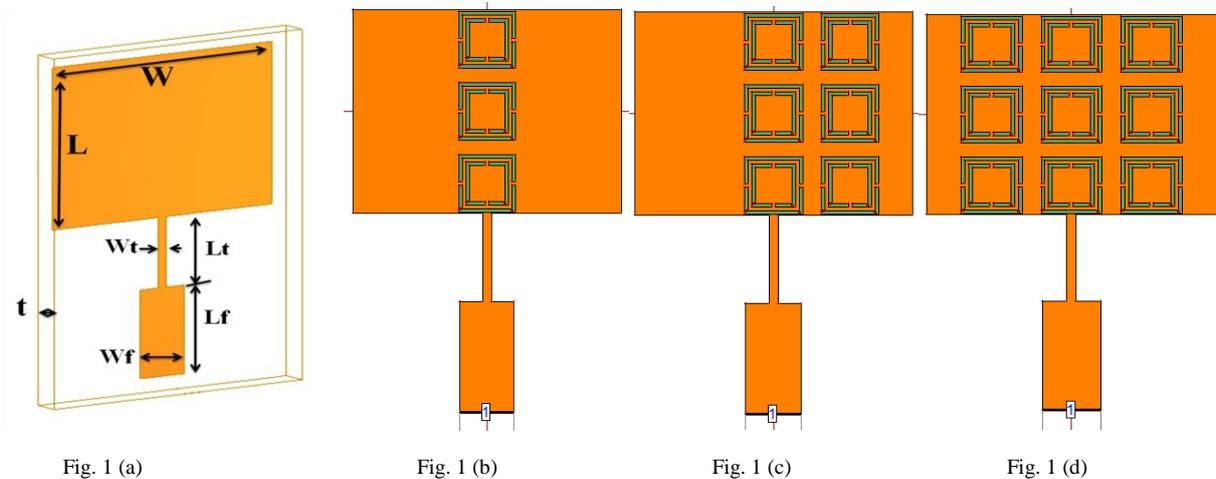


Fig.1: Geometry of proposed microstrip patch antenna (a) Conventional (b) back view of antenna1 (c) back view of antenna2 and (d) back view of antenna3

Parameters	Size (mm)
Length of the patch(L)	11.35
Width of the patch(W)	15.25
Length of the quarter wave transformer(Lt)	4.90
Width of the quarter wave transformer(Wt)	0.50
Length of the 50 Ω line(L50)	6.15
Width of the 50 Ω line(W50)	3.05
Length of the ground plane(Lg)	40
Width of the ground plane(Wg)	40

Table 1: Various dimensions of patch and ground plane

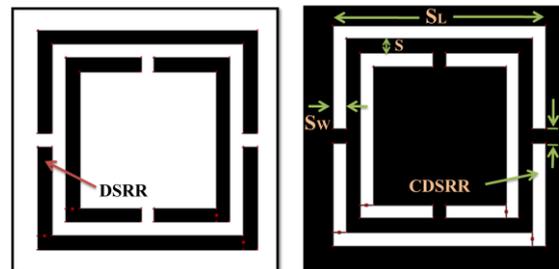


Fig. 2(a) A dual split ring resonator (b) Complementary dual split ring resonator with the design parameters

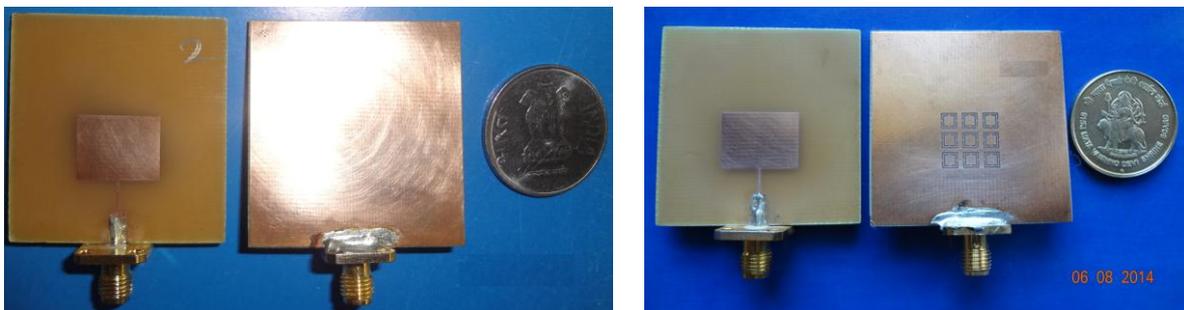


Fig. 3 (a)

Fig.3 (b)

Fig. 3 (a) photographic view of the proposed conventional microstrip patch antenna and 3(b) Antenna 3

III. RESULTS AND DISCUSSIONS

The simulation is carried out by using the mentor graphics IE3D simulation software version 14.65. The parameters of the proposed antennas are measured on Vector Network Analyzer (VNA) (Rhode and Schwarz, Germany make ZVK model 1127.8651).

Fig. 4 shows the simulated return loss characteristics of conventional microstrip antenna, Antenna 1, Antenna 2 and Antenna 3. From this figure it is seen that, conventional microstrip antenna resonates at 5.90GHz and the optimized Antenna 3 is resonating at 5.31GHz. The impedance bandwidth over return loss less than -10dB is determined by using the equation

$$BW = \left[\frac{f_2 - f_1}{f_c} \right] \times 100 \%$$

Where, f_1 and f_2 are the lower and upper cut-off frequencies of the band respectively, when its return loss reaches -10dB and f_c is the centre frequency between f_1 and f_2 . All the parameters of simulated results are tabulated in table 2.

Initially, the return loss characteristic of conventional antenna is compared with fabricated conventional antenna and which is shown in Fig. 5. The practically measured conventional antenna is resonating at $f_r = 5.98$ GHz with 250 MHz of bandwidth. In the next step the optimized CDSRRs loaded antenna 3 is fabricated and measured, which is resonating at two different frequency points as $f_{r1} = 5.32$ GHz and $f_{r2} = 9.45$ GHz with bandwidths of 180 MHz and 990 MHz respectively. The measured return loss characteristics are compared with that of simulated values and the results are shown in table 3. Fig. 7 shows the simulated and measured return loss characteristics of the antenna 3. It is observed from the figures that, the simulated and measured results are in good agreement with each other.

Fig. 7(a) and Fig. 7(b) show the radiation patterns of conventional microstrip antenna and antenna 3 at their operating bands. From these figures it is seen that, the patterns are broadside in nature in both the cases.

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 2, Issue 8, August 2014

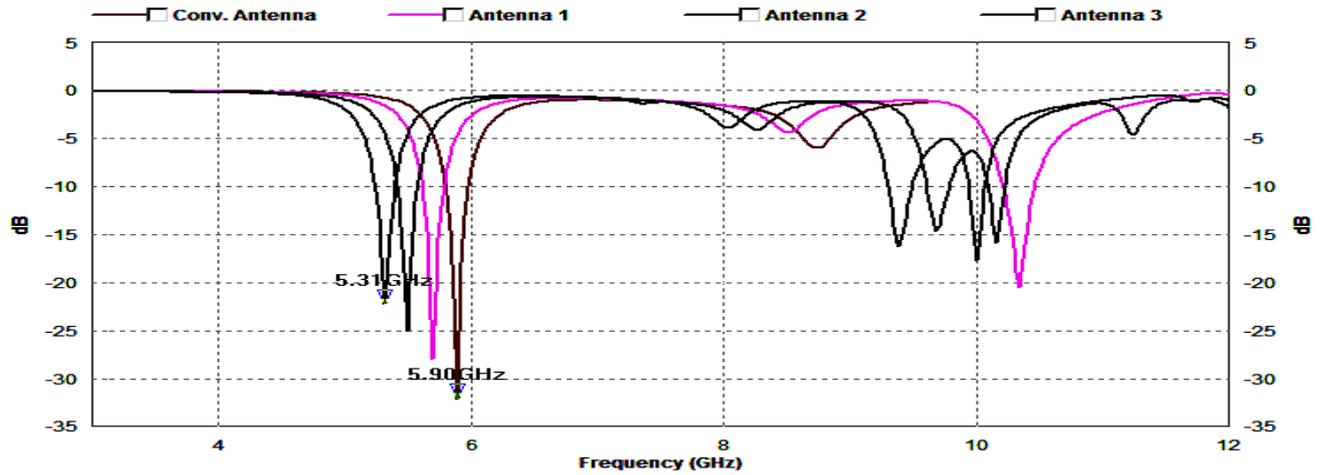


Fig. 4: Return loss characteristics of proposed antennas with and without DSCSRR

Antenna configurations	Resonating Frequency (GHz)	Minimum Reflection Co-efficient (dBi)	Band Width (MHz)	Bandwidth (%)	Size Reduction (%)
Conventional Antenna	5.90	-33.95	180	2.99	-
Antenna 1	5.69 10.33	-27.89 -20.89	171 249	3.00 2.41	3.5
Antenna 2	5.49 9.68 10.15	-25.03 -14.68 -15.83	162 179 131	2.95 1.84 1.29	6.91
Antenna 3	5.31 9.38 9.99	-22.29 -16.22 -17.71	158 193 130	2.97 2.05 1.30	9.95

Table 2: Simulated results of proposed antennas

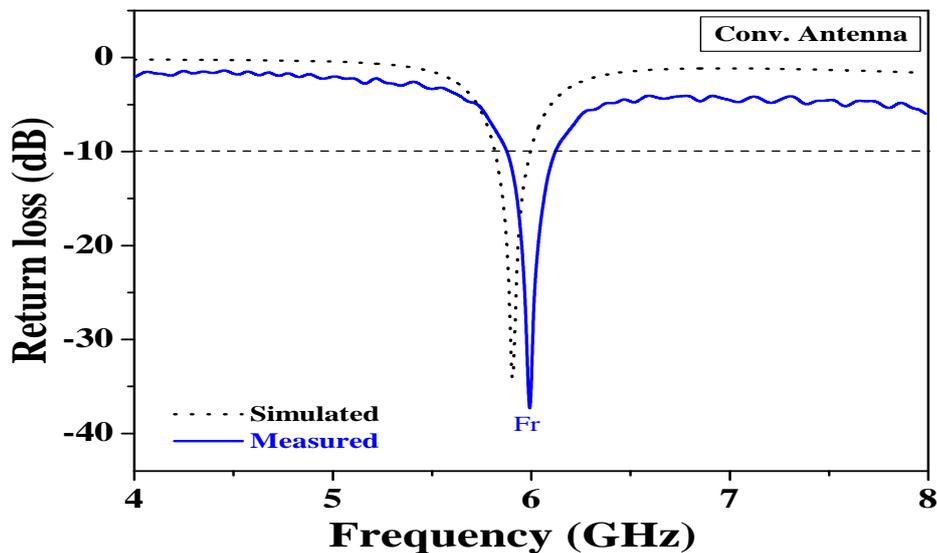


Fig. 5: Simulated and measured return loss characteristics of conventional antenna

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 2, Issue 8, August 2014

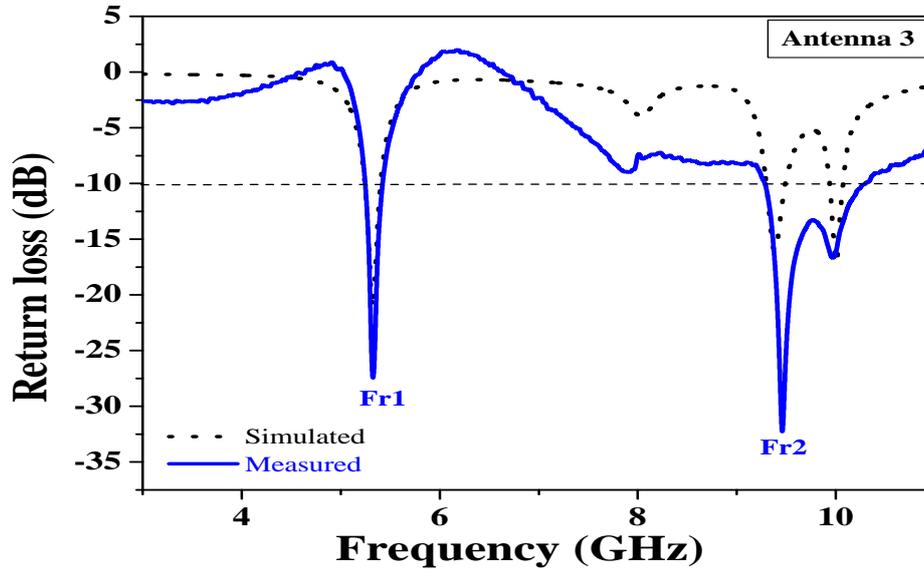


Fig. 6: Simulated and measured return loss characteristics of antenna 3

Antenna configurations	Resonating Frequency (GHz)		Minimum Reflection Co-efficient (dBi)		Band Width (MHz)		Overall Bandwidth (%)		Size Reduction (%)	
	Sim	Pract	Sim	Pract	Sim	Pract	Sim	Pract	Sim	Pract
Conventional Antenna	5.90	5.97	-33.95	-42.40	180	240	3.05	4.02	---	--
Antenna 3	5.31	5.32	-22.29	-27.33	158	180	6.32	13.85	9.95	10.86
	9.38	9.45	-16.22	-31.29	193	990				
	9.99	--	-17.71	---	130	---				

Table 3: Comparison of simulated and measured results of Conv. Antenna and antenna 3

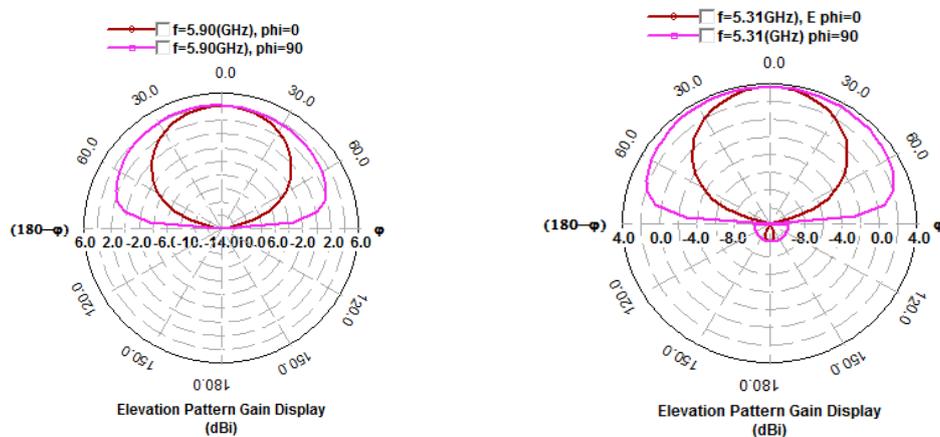


Fig. 8(a) Radiation pattern at 5.90GHz of conventional antenna (b) at 5.31GHz of antenna 3



ISSN(Online): 2320-9801
ISSN (Print): 2320-9798

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 2, Issue 8, August 2014

IV. CONCLUDING REMARKS

In this work a design of metamaterial antenna based on CDSRRs has been proposed. Because of the inclusion of CDSRRs, the conventional microstrip antenna previously resonating at one frequency produces two working frequencies now. At each frequency, good matching and size reduction is obtained. A good agreement between simulated and measured results validates our design. The proposed CDSRRs antenna provides us a new way to design multi-band antennas. Besides, thanks to the presence of the CDSRRs, a size reduction and enhanced bandwidth of microstrip antenna can be achieved.

ACKNOWLEDGEMENT

The authors acknowledge their thanks to UGC, New Delhi for sanctioning the IE3D simulation software under Major Research Project, which is most useful and reliable for designing microstrip antennas and DST, New Delhi for sanctioning Vector Network Analyzer for measuring the parameters of fabricated antenna.

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BIOGRAPHY



Mr. Prashant R T received his M Sc from the department of Applied Electronics Gulbarga University, Gulbarga in the year 2011. He worked as a Project Fellow in the UGC sponsored Major Research Project during the year 2012-2013. Currently he is pursuing his Ph. D in the field of Microwave Antennas from the department of Applied Electronics, Gulbarga University, Gulbarga.



Dr. Vani R M received her B.E. in Electrical and Electronics from the B.I.E.T., Davanagere and M.Tech in Industrial Electronics from S.J.C.E., Mysore, Karnataka. She has received her Ph.D in Applied Electronics from Gulbarga University, Gulbarga, India, in year 2005. She is working as Reader & Head, University Science Instrumentation Centre, Gulbarga University, Gulbarga, since 1995. She has more than 85 research publications in national and international reputed Journals/Conference proceedings. She presented the research papers in National/ International conferences in India and abroad. She has conducted several courses, workshops for the benefits of faculties and field engineers. Her areas of interest are microwave antennas, PC

based instrumentation, embedded controllers and Wireless communication. She has one UGC

major research project to her credit.



Dr. P V Hunagund received his M.Sc and Ph.D from the Dept. of Applied electronics, Gulbarga University, Gulbarga, in the year 1982 and 1992 respectively. He is working as professor and chairman of Applied Electronics department, Gulbarga University, Gulbarga. He has more than 100 research publications in national and international reputed journals, more than 200 research publications in international symposium/Conferences. He presented the research papers in National/International conferences in India and abroad. He has guided many Ph.D and M.Phil students. He has three major research projects at his credit.