



(An ISO 3297: 2007 Certified Organization) Vol. 3, Issue 3, March 2014

Corrosion Inhibition of Aluminum in Hydrochloric Acid Solutions Using Some Chalcone Derivatives

A. S. Fouda*, K. shalabi, N. H. Mohamed

Department of Chemistry, Faculty of Science, El-Mansoura University, El-Mansoura-35516, Egypt

Abstract: The inhibition effect of some Chalcone derivatives [3-(4-hydroxyphenyl)-1-phenylprop-2-en-1-one as an inhibitor (1) and 3-(4-hydroxyphenyl)-1-(4-nitrophenyl)prop-2-en-1-one as an inhibitor (2)] on the corrosion of aluminum in 0.5 M HCl solution was studied using potentiodynamic polarization, electrochemical impedance spectroscopy (EIS), electrochemical frequency modulation (EFM) and weight loss measurements. The results drawn from the different techniques are comparable and exhibit small discrepancy. Results for weight loss indicated that inhibitor efficiency (% IE) increased with increasing inhibitor concentration, reaching a maximum inhibiting power of 85.9, 95.7 % at 21 x 10^{-6} M for inhibitors 1 and 2, respectively and decreased with increasing the temperature. Polarization studies clearly revealed that the presence of inhibitors changes the mechanism of hydrogen evolution and the metal dissolution i.e. they act as mixed type inhibitors. Some activation and adsorption thermodynamic parameters were calculated and discussed. The surface coverage of the inhibitors obeyed Langmuir adsorption isotherm.

Keywords: Chalcone derivatives, Aluminum, HCl, Potentiodynamic polarization, EIS, EFM, Langmuir isotherm

I. INTRODUCTION

Aluminum is one of the metals which used in different human activities and many of important applications, where it is the second most abundant metal after iron, it has a low atomic mass and negative value of standard electron potential, aluminum potentially attracts as an anodic material for power sources with high energy density. It is used in construction, packing and transportation because of its strength and electrical conductivity. Aluminum is used in electronics due to it is super purity [1]. Although Al has an adhesive protective passivating oxide film, but this film has an amphoteric susceptibility, and consequently the metal dissolves readily in acidic and basic solutions concentrated above and below pH 4-9 [2, 3]. In our efforts to mitigate electrochemical corrosion of aluminum, the main strategy is to isolate the metal from corrosive agents and this can be achieved by using corrosion inhibitors which prevent the adsorption of the aggressive anions or by the formation of a more resistance oxide film on the metal surface. Generally, it has been assumed that the first stage in the action mechanism of the inhibitors in aggressive acid media as hydrochloric acid is the adsorption of the inhibitors on the metal surface where HCl solutions are used for pickling of aluminum for its chemical or electrochemical etching [4]. Various mechanisms have been proposed to explain the breakdown of the passive oxide film when chloride reach the metal film interface. Recently, has shown that chloride does not enter the oxide film but it is chemisorbed on the oxide surface [5] and act as a reaction partner, aiding dissolution via the formation of oxide-chloride complexes. Among several methods used in combating corrosion problems, the use of chemical inhibitors remains the most cost effective and practical method [6, 7]. From this point of view, a great number of investigators have conducted research work to find effective inhibitors for aluminum corrosion in harsh environments [8-10]. Some reported the effect of inorganic oxidants [8], while others studied the use of organic compounds [11-14]. It is well known that azole derivatives like benzotriazole, mercaptoben, benzimidazole and imidazole can be employed as inhibitors against corrosion for many metals and alloys. Azole compounds have been used to protect the corrosion of aluminum [15] in corrosive environments. In general, organic compounds with oxygen, sulfur, and/or nitrogen as polar groups and conjugated double bonds in their structures have been reported to be good corrosion inhibitors for many metals and alloys in corrosive media [16-32]. The inhibiting action of these organic compounds is usually attributed to their interactions with the metallic surfaces via their adsorption. Polar functional



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

groups are regarded as the reaction center that stabilitizes the adsorption process [6]. However, the adsorption of an inhibitor on a metal surface depends on a few factors, such as the nature and surface charge of the metal, the adsorption mode, the inhibitor's chemical structure, and the type of the electrolyte solution [33].

In this work, we investigate the effect of some chalcone derivatives on the corrosion behavior of aluminum in 0.5 M HCl solution using chemical, electrochemical techniques and quantum chemical calculations.

II. EXPERIMENTAL

2.1. Materials and reagents

Aluminum sheets with purity more than 98.8 % were used in this study. The aggressive solution, 0.5 M HCl was prepared by dilution with bidistilled water. The chalcone derivatives were synthesized according to the procedures described in previous paper [34] and are presented in Table 1. 10^{-6} M stock solutions from the investigated compounds were prepared by dissolving the appropriate weights of the used chemically pure solid compounds in absolute ethanol.

Table 1: structures, molecular weights and molecular formulas of the investigated Chalcone derivatives

	Names	Structures	Molecular weights & Chemical formulas	
1	3-(4-hydroxyphenyl)-1- phenylprop-2-en-1-one		224.25 C ₁₅ H ₁₂ O ₂	
2	3-(4-hydroxyphenyl)-1-(4- nitrophenyl)prop-2-en-1-one	О2N ОН	269.25 C ₁₅ H ₁₁ NO ₄	

2.2. Weight loss measurements

The Seven parallel aluminum sheets of $(2.4 \times 2.5 \times 0.1 \text{ cm})$ were abraded with emery paper (grade uo to 1200 grit size) and then washed with bidistilled water and acetone. After accurate weighing, the specimens were immersed in a 250 ml beaker, which contained 100 ml of HCl with and without addition of different concentrations of the investigated compounds. All the aggressive acid solutions were open to air and the measurement was conducted at room temperature $(25 \pm 1 \text{ °C})$. After 5 h, the specimens were taken out, washed, dried, and weighed again accurately. The average weight loss of seven parallel aluminum sheets could be obtained. The inhibition efficiency (% IE) and the degree of surface coverage, θ , of investigated compounds for the corrosion of aluminum in HCl were calculated as follows [35]:

% IE =
$$\theta \times 100 = [(Wo - W)/Wo] \times 100$$

(1)

where Wo and W are the values of the average weight losses in the absence and presence of the inhibitor, respectively.

2.3. Electrochemical measurements

The experiments were carried out potentiodynamically in three electrode cell. Platinum foil was used as counter electrode and a saturated calomel electrode (SCE) coupled to a fine Luggin capillary as the reference electrode. The working electrode was in the form of a square cut from aluminum sheet under investigation and was embedded in a Teflon rod with an exposed area of 1 cm². This electrode was immersed in 100 ml of a test solution for 30 min until a steady state open-circuit potential (E_{ocp}) was attained. The potentiodynamic curves were recorded by changing the electrode potential from -0.5 to 1.5 V versus SCE with scan rate of 1 mV/s. All experiments were carried out in freshly prepared solution at room temperature (25°C) using a thermostat. % IE and the degree of surface coverage (θ) were calculated from Eq. (2):



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

% IE = $\theta \times 100 = [1 - (i_{corr(inh)} / i_{corr})] \times 100$

(2)

where $(i_{corr,})$ and $i_{corr(inh)}$ are the uninhibited and inhibited corrosion current density values, respectively, determined by extrapolation of Tafel line.

The electrochemical impedance spectroscopy (EIS) spectra were recorded at open circuit potential (OCP) after immersion the electrode for 30 min in the test solution. The ac signal was 5 mV peak to peak and the frequency range studied was between 100 kHz and 0.1 Hz. The main parameters deduced from the analysis of Nyquist diagram are the polarization resistance R_p and the capacitance of double layer (C_{dl}) which is calculated from Eq.(3): $C_{r} = \frac{1}{2} \left(2\pi f - R_p \right)$

$$C_{dl} = 1/(2 \pi f_{max} R_P)$$

where (f_{max}) is the angular frequency at which the imaginary component of the impedance reaches its maximum values. The inhibition efficiency (%IE) and the surface coverage (θ) of the used inhibitors obtained from the impedance measurements were calculated by applying the following relations:

% IE =
$$\theta \times 100 = [1 - (R_p^{\circ}/R_p)] \times 100$$

(4)

Where R_p° and R_p are the polarization resistance in the absence and presence of inhibitor, respectively. Electrochemical frequency modulation (EFM) is a non-destructive corrosion measurement technique that can directly give values of the corrosion current without a prior knowledge of Tafel constants. Like EIS, it is a small signal ac technique. Unlike EIS, however, two sine waves (at different frequencies) are applied. The intermodulation spectra contain current responses assigned for harmonically and intermodulation current peaks. The larger peaks were used to calculate the corrosion current density (i_{corr}), the Tafel slopes (β_c and β_a) and the causality factors CF-2& CF-3 [36,37]. The electrode potential was allowed to stabilize for 30 min before starting the measurements. All the experiments were conducted at 25± 1°.

All electrochemical measurements were carried out using Potentiostat /Galvanostat/ Zra analyzer (Gamry PCI300/4). A personal computer with DC105 software for potentiodynamic, EIS300 software for EIS and EFM140 software for EMF and Echem Analyst 5.21 was used for data fitting.

2.4. Surface morphology

For morphological study, surface features (2.0 cm x 2.0 cm x 0.15 cm) of aluminum were examined before and after exposure to 0.5 M HCl solutions for 24 hour with and without inhibitor. JEOL JSM-5500 scanning electron microscope was used for this investigation.

III. RESULTS AND DISCUSSION

3.1. Weight loss measurements

Weight The corrosion rate of aluminum as a function of time and temperature were investigated. Fig (1) represents the weight loss-time curves in the absence and presence of different concentrations of inhibitor (2) at 25° C (the more effective inhibitor). Similar curves were obtained for the other inhibitor (not shown). It is obvious that the uniformity and non-linearity of the plot in the absence of inhibitor suggest that the aluminum corrosion in HCl is a heterogeneous process involving several steps. Similar observations have been reported for aluminum corrosion in other media [38]. The corrosion of aluminum in HCl in the presence of inhibitor shifted to more uniform and more linear plots, and is much lower than in case of absence of inhibitor. The inhibitor molecules were shown in Tables (2). The %IE increases with increasing the inhibitor concentration indicated that more inhibitor molecules are adsorbed on the metal surface thus providing wider surface coverage. The optimum concentration required to achieve an efficiency of 95.75% and 85.88% was found to be 21×10^{-6} M for inhibitors 1 &2, respectively.



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014



Fig. 1: Weight loss- time curves for aluminum corrosion at different concentrations of inhibitor (2) after 180 min immersion in 0.5 M HCl at 25°C

Table 2: Inhibition efficiency (% IE) and surface coverage (Θ) at different concentrations chalcone derivatives for the corrosion of aluminum after 180 min immersion in 0.5 M HCl at 25°C

Concentration,	Inhibi	tor (1)	Inhibitor (2)				
IVI	% IE	θ	% IE	θ			
1X10 ⁻⁶	67.54	0.6754	72.7	0.727			
5X10 ⁻⁶	73.53	0.7353	76.0	0.760			
9X10 ⁻⁶	75.66	0.7566	79.1	0.791			
13X10 ⁻⁶	76.95	0.7695	85.7	0.857			
17X10 ⁻⁶	79.41	0.7941	92.8	0.928			
21X10 ⁻⁶	85.88	0.8588	95.7	0.957			

3.2. Adsorption isotherms

Corrosion inhibitors are found to protect aluminum corrosion in acid solutions by adsorbing themselves on aluminum surface where the adsorption of the organic molecules occurs as the interaction energy between molecule and metal surface is higher than that between the water molecules and the surface [39], and it is regarded as substitution adsorption process between the organic molecules in the aqueous phase (org_{aq}) and the water molecules adsorbed on the aluminum surface (H₂O)_{ads} [40].

$$xH_2O_{ads} + Org_{sol} \iff Org_{ads} + xH_2O$$

5)

(6)

where x is the size ratio, that is, the number of water molecules replaced by one organic molecule. Inhibitors molecules are either physically or chemically adsorbed on a corroding metal surface, where the physisorbed molecules retard metal dissolution by inhibiting the cathodic reaction whereas chemisorbed molecules inhibit the anodic reaction by reducing the inherent reactivity of the metal at the adsorption sites [41]. It was found that the best suitable adsorption isotherm for the studied inhibitors on the aluminum surface is the Langmuir equation [42] which was defined as follows:

$$C/\Theta = 1/K_{ads} + C$$

where K_{ads} is equilibrium constant of adsorption process, and C is concentration of inhibitor. The plot of \dot{C}/Θ versus C for the inhibitors are shown (Figs. 2a,2b) to be linear with slope near unity, and correlation coefficients near to unity in order to obtain the isotherm. The thermodynamic adsorption parameters were calculated. The well-known thermodynamic adsorption parameters are the standard free energy of adsorption (ΔG°_{ads}), the heat of adsorption (ΔH°_{ads}) and the entropy of adsorption (ΔS°_{ads}). These quantities can be calculated by various mathematical methods depending on the values of K_{ads} from adsorption isotherms at different temperatures [43]. The ΔG°_{ads} can be calculated from Eq. (7):

$$K_{ads} = (1/55.5) \exp \left(-\Delta G^{\circ}_{ads} / RT\right)$$

(7)



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

where 55.5 is the concentration of water in mol Γ^{1} , R is the universal gas constant, and T is the absolute temperature. (ΔH°_{ads}) , (ΔS°_{ads}) can be calculated from Eqs (8 &9):

 $Log K_{ads} = (\Delta H^{o}_{ads} / 2.303 RT) + constant$

 $\Delta G^{\circ}_{ads} = \Delta H^{\circ}_{ads} - T\Delta S^{\circ}_{ads}$

(8) (9)

Table (3) shows all the estimated thermodynamic adsorption parameters for the chalcone derivatives on aluminum surface, and concluded that: Large values of K_{ads} mean good inhibition efficiency of the inhibitors and strong electrical interaction between the adsorbate and the adsorbent. The sign of ΔG°_{ads} was negative which reflects that the adsorption of these inhibitors is spontaneous process. It is well known that values of ΔG°_{ads} of the order of 40 kJ mol⁻¹ or higher involve charge sharing or transfer from the inhibitor molecules to metal surface to form coordinate type of bond (chemisorption); those of order of 20 kJ mol⁻¹ or lower means that the electrostatic interaction between metal surface and charged organic molecules in the bulk of the solution indicate a physisorption [44, 45]. The calculated ΔG°_{ads} values are above 40 kJ mol⁻¹ which indicate that the adsorption mechanism of the investigated compounds on aluminum in 0.5 M HCl solution is a chemisorption and shifted to physisorption by increasing temperature, so it is a comprehensive adsorption (physical and chemical). ΔG°_{ads} values increase (become less negative) with an increase in temperature which indicate that the adsorption process is an exothermic process. The negative sign of ΔH°_{ads} indicates that the adsorption process of both inhibitors molecules is an exothermic process. Generally, an exothermic adsorption process suggests either physisorption or chemisorption while endothermic process is attributed to chemisorption [46]. Generally, enthalpy values up to 41.9 kJ.mol⁻¹ are related to physisorption while those around 100 kJ.mol⁻¹ or higher are attributed to chemisorption. The unshared electron pairs in investigated molecules may interact with p-orbital of aluminum to provide chemisorbed film. The values of ΔS°_{ads} are large and negative that is accompanied with exothermic adsorption process.



Fig. 2.a Langmuir adsorption isotherm of inhibitor (1) on aluminum surface in 0.5 M HCl at different temperatures





(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014



С, М

Fig. 2.b Langmuir adsorption isotherm of inhibitor (2) on aluminum surface in 0.5 M HCl at different temperatures Table (3) Thermodynamic parameters for the adsorption of inhibitors on aluminum surface in 0.5 M HCl at different temperatures

Inhibitor	Temp, °C	$\frac{K_{ads} x 10^{-3}}{M^{-1}}$	$-\Delta G^{\circ}_{ads,}$ kJ mol ⁻¹	-ΔH° _{ads} , kJ mol ⁻¹	$-\Delta S^{\circ}_{ads},$ J K ⁻¹ mol ⁻¹
1	25	1040.6	44.29	52.42	27.30
1	45	275.0	43.74	52.42	27.30
2	25	759.2	43.50	60.92	58.46
2	45	1195.2	42.62	60.92	57.55

3.3. Effect of temperature

The importance of temperature variation in corrosion study involving the use of inhibitors is to determine the mode of inhibitor adsorption on the metal surface. Recently, the use of two temperatures to establish the mode of inhibitor adsorption on a metal surface has been reported and has been found to be adequate. Thus, the influence of temperature on the corrosion behavior of aluminum in 0.5 M HCl in the absence and presence of the investigated compounds by hydrogen evolution method at 25 and 45 °C. Therefore, in examining the effect of temperature on the corrosion process, the apparent activation energies (E_a) were calculated from the Arrhenius equation [47].

Log ($k_{2 \text{ corr}} / k_{1 \text{ corr}}$) = ($E_a / 2.303 \text{R}$) x ($1/T_1 - 1/T_2$)

(10)

where k_{1corr} and k_{2corr} are the corrosion rates at temperature T_1 and T_2 , respectively. An estimate of heat of adsorption was obtained from the trend of surface coverage with temperature as follows [48]:

$$Q_{ads} = 2.303R [log (\Theta_2/1 - \Theta_2) - log (\Theta_1/1 - \Theta_1)] x (T_1 T_2 / T_2 - T_1)$$

(11)

where Θ_1 and Θ_2 are the degrees of surface coverage at temperatures T_1 and T_2 , The calculated

values for both parameters are given in Table 4. Increased activation energy (E_a) in inhibited solutions compared to the blank suggests that the inhibitor is physically adsorbed on the aluminum metal surface [49]. It is seen from Table 4 that E_a values rose with increasing the inhibitor concentration, suggesting strong adsorption of the investigated inhibitors on the aluminum metal surface. It has been suggested that adsorption of an organic inhibitor can affect the corrosion rate by either decreasing the available reaction area (geometric blocking effect) or by modifying the activation energy of the anodic or cathodic reactions occurring in the inhibitor-free surface in the course of the inhibited corrosion process [50] The negative sign Q_{ads} values indicate that the adsorption process and the degree of surface coverage decreased with increasing in temperature, supporting the physisorption mechanism [51].

Table 4: The activation energy (E_a) and the heat of adsorption (Q_{ads}) for aluminum dissolution in 0.5 M HCl in the absence and presence of inhibitors at 25 and 45°C



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

	Inhil	bitor (1)	Inhibitor (2)			
Concentration, M	E _{a,} kJ mol ⁻¹	-Q _{ads} kJ mol ⁻¹	E _{a,} kJ mol ⁻¹	-Q _{ads} kJ mol ⁻¹		
Blank	49.97		49.97			
1x10 ⁻⁶	70.85	37.01	50.84	1.22		
5x10 ⁻⁶	72.46	35.27	52.89	3.85		
9x10 ⁻⁶	71.68	32.32	54.10	5.36		
13x10 ⁻⁶	69.07	27.25	60.09	12.03		
17x10 ⁻⁶	58.63	11.25	83.90	38.31		
21x10 ⁻⁶	70.61	29.71	96.91	51.24		

3.5. Potentiodynamic polarization measurements

The potentiodynamic polarization curves of aluminum in 0.5 M HCl solutions containing different concentrations of investigated compounds at 25°C are shown in Figs. (3.a, 3.b) for inhibitors 1, 2 respectively. The corrosion kinetic parameters such as corrosion current density (i_{corr}), corrosion potential (E_{corr}), the anodic Tafel slopes (β_a) and cathodic Tafel slope (β_c), degree of surface coverage (Θ) and the inhibition efficiency (%IE) of both inhibitors are shown in Table 5 for the aluminum in 0.5 M HCl solution in the absence and presence of different concentrations of the both inhibitors are listed in Table 5. The results of this Table indicated that the corrosion current density (i_{corr}) decreases in the presence of inhibitors compared to the blank solution and also with increasing the inhibitors concentrations which suggest that the presence of these compounds retard the dissolution of aluminum in 0.5 M HCl solution. Presence of these inhibitors cause decrease in the corrosion rate, so shift both the anodic and cathodic curves to lower values of current densities. This implies that both the hydrogen evolution and the anodic dissolution of aluminum metal are inhibited. This due to adsorption of the inhibitors over the corroding surface [52, 53]. The slopes of the anodic and cathodic Tafel lines (β_a , β_c) were slightly changed on increasing the concentration of the investigated compounds. This means that there is no change of the mechanism of the inhibition in presence and absence of inhibitors and that inhibitors affects both anodic and cathodic reactions, so it is mixed type inhibitors. Inhibition efficiency (%IE) was calculated from equation (2). The order of % IE was found to decrease in the following sequence: inhibitor 2 > 2inhibitor 1.



Fig. 3a: Potentiodynamic polarization curves for the corrosion of aluminum in 0.5 M HCl in the absence and the presence of various concentrations of inhibitor (1) at 25 °C



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014



Fig. 3b: Potentiodynamic polarization curves for the corrosion of aluminum in 0.5 M HCl in the absence and the presence of various concentrations of inhibitor (2) at 25° C

Table 5: Potentiodynamic	polarization	parameters	for th	e corrosion	of	aluminum	in	0.5	Μ	HCl	in	the	absence	and	presence	of	different
concentrations of investiga	ted compound	ls															

Inh.	Conc., M	-E _a , mV vs. SEC	i_{corr} , mA cm ⁻²	$\beta_{a,-1}$	$\beta_c,$ V dec	CR mmy ⁻¹	θ	% IE
Blank	0.0	724	222.00	4.30	8.27	2451		
	1×10^{-6}	724	99.06	4.00	9.52	940	0.5550	55.50
	5x10 ⁻⁶	723	69.43	3.03	8.91	881	0.6881	68.81
(1)	9x10 ⁻⁶	722	47.30	2.55	3.78	598	0.7280	72.80
	13x10 ⁻⁶	725	42.85	1.50	6.26	442	0.8075	8.75
	17x10 ⁻⁶	713	38.20	0.89	1.03	166	0.8284	82.84
	21x10 ⁻⁶	734	23.51	0.48	1.46	102	0.8944	89.44
	1x10 ⁻⁶	721	65.33	2.18	4.8	518	0.8752	87.52
	5x10 ⁻⁶	697	54.00	0.88	2.39	463	0.9387	93.87
(2)	9x10 ⁻⁶	744	47.37	0.05	0.24	312	0.9562	95.62
(2)	13x10 ⁻⁶	745	36.64	0.05	0.25	202	0.9687	96.87
	17x10 ⁻⁶	747	21.06	0.04	0.21	187	0.9811	98.11
	21×10^{-6}	749	6.12	0.06	0.25	149	0.9902	99.02

3.6. Electrochemical impedance spectroscopy (EIS) measurements

The corrosion behavior of aluminum in 0.5 M HCl solution in the absence and presence of different concentrations of the inhibitors was investigated by the EIS method at 25 °C after 30 min of immersion. Figs. (4.a, 4.b) show the Nyquist plot for aluminum in 0.5 M HCl solution in the absence and presence of different concentrations of investigated compounds. The fact that impedance diagrams have an approximately semi-circular appearance shows that the corrosion of aluminum in 0.5 M HCl is controlled by a charge transfer resistance process. Small distortion was observed in some diagrams, this distortion has been attributed to frequency dispersion [54] as a result of surface roughness, impurities, dislocations, grain boundaries, adsorption of inhibitors and formation of porous layers and inhomogeneity of the electrode surface. The electrical equivalent circuit model which describes the metal / electrolyte interface of the present corroding system is shown in Fig. 5. The model consists of the solution resistance (R_s), the charge-transfer resistance of the interfacial corrosion reaction (R_{ct}), and the double layer capacitance (C_{dl}). Table 6 shows the EIS data where the C_{dl} values decrease and the R_{ct} values increase with the increase of the inhibitor molecules



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

on the metal surface, and decreasing the extent of dissolution reaction. The high (R_{ct}) values are generally associated with slower corroding system [55, 56]. The decrease in the C_{dl} can result from the decrease of the local dielectric constant and/or from the increase of thickness of the electrical double layer [57] suggested that the inhibitor molecules function by adsorption at the metal/solution interface. The % IE obtained from EIS measurements are close to those deduced from polarization method. The order of inhibition efficiency obtained from EIS measurements is as follows: inhibitor 2 > inhibitor 1



Fig. 4: Electrical equivalent circuit used to fit the impedance data



Fig. 4a: Nyquist plots for the corrosion of aluminum in 0.5 M HCl in the absence and the presence of different concentrations of inhibitor (1) at 25°C



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014



Fig. 4b: Nyquist plots for the corrosion of aluminum in 0.5 M HCl in the absence and the presence of different concentrations of inhibitor (2) at 25° C

estigated compoun	ds at 25 C				
Comp.	Conc.,	$C_{dl}x10^{-5}$,	R _{ct} ,	θ	% IE
	М	$\mu F \text{ cm}^{-2}$	$\Omega \ { m cm}^2$		
Blank	0.0	40.30	2.28		
	1×10^{-6}	40.00	5.84	0.6094	60.94
	5x10 ⁻⁶	34.00	8.27	0.7244	72.44
1	9x10 ⁻⁶	23.90	10.75	0.7880	78.80
	13x10 ⁻⁶	13.20	12.49	0.8174	81.74
	17x10 ⁻⁶	12.50	16.17	0.8590	85.90
	21x10 ⁻⁶	12.40	19.30	0.8819	88.19
	1x10 ⁻⁶	39.40	7.30	0.6875	68.75
	5x10 ⁻⁶	37.00	9.05	0.7481	74.81
2	9x10 ⁻⁶	35.70	11.97	0.8095	80.95
2	13x10 ⁻⁶	34.10	20.48	0.8887	88.87
	17x10 ⁻⁶	32.60	52.78	0.9568	95.68
	21x10 ⁻⁶	21.10	205.40	0.9889	98.89

Table 6: Electrochemical kinetic parameters obtained from EIS technique for the corrosion of aluminum in 0.5 M HCl at different concentrations of investigated compounds at 25 C

3.7. Electrochemical frequency modulation (EFM) measurements

The EFM is a nondestructive corrosion measurement technique that can directly give values of the corrosion current without prior knowledge of Tafel constants. It is generally accepted that in most cases, the corrosion rates determined with the EFM technique, are much higher than the values determined with other techniques exhibiting low corrosion rates (58). The modulation frequencies that are used in the EFM technique are in the capacitive region of the impedance spectra. However, results of the EFM technique showed good agreement of corrosion rates obtained with the Tafel extrapolation method. Figs. 5 are example of aluminum immersed in 0.5 M HCl solutions and in presence of 21 x10⁻⁶ M inhibitor (2) as an example at 25°C. Each spectrum is a current response as a function of frequency. Table 5 shows the calculated corrosion kinetic parameters at different concentrations of the investigated compounds in 0.5 M HCl at 25°C ($i_{corr,} \beta_a, \beta_c, CF-2, CF-3$ and % IE). From Table 4, the corrosion current densities decrease by increasing investigated compounds concentrations. The causality factors in Table 7 are very close to theoretical values, which according to EFM theory [59] should guarantee the validity of Tafel slopes and corrosion current densities. Values of causality factors in Table 7 indicate that the measured data are of good quality. The standard values for CF-2 and CF-3 are 2.0



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

and 3.0, respectively. The deviation of causality factors from their ideal values might be due to the perturbation amplitude which was too small or that the resolution of the frequency spectrum is not high enough. Another possible explanation is that the inhibitor is not performing very well. The obtained results showed good agreement of corrosion kinetic parameters obtained with the EFM, Tafel extrapolation and EIS methods.

Table 7: Electrochemical kinetic parameters obtained by EFM technique for aluminum in 0.5 M HCl solutions containing various concentrations of the investigated compounds at 25 °C

Concentration, M		i _{corr} , μA cm ⁻²	β_a mV dec ⁻¹	β_c mV dec ⁻¹	CR mpy	CF-2	CF-3	θ	% IE
Bl	lank	930.30	142	446	560.4	1.5	2.23		
	1x10 ⁻⁶	361.70	27.90	89.40	156.9	1.9	2.6	0.6112	61.12
	5x10 ⁻⁶	223.10	20.30	26.70	96.77	1.7	3.2	0.7202	72.02
(1)	9x10 ⁻⁶	221.71	19.70	26.80	96.01	2.8	3.2	0.7420	74.20
(1)	13x10 ⁻⁶	215.92	20.00	24.30	93.63	1.6	2.4	0.7679	76.79
	17x10 ⁻⁶	214.71	19.70	24.10	93.12	1.5	3.1	0.7692	76.92
	21x10 ⁻⁶	210.81	20.40	21.90	91.40	2.1	3.1	0.7734	77.34
	1x10 ⁻⁶	269.41	67.30	94.60	116.80	1.16	3.48	0.7104	71.04
	5x10 ⁻⁶	252.02	71.20	99.60	109.30	1.01	2.48	0.7291	72.91
(2)	9x10 ⁻⁶	233.97	22.80	27.70	139.40	2.87	3.28	0.7485	74.85
(=)	13x10 ⁻⁶	215.55	19.80	24.40	129.80	1.77	2.99	0.7683	76.83
	$17x10^{-6}$	166.43	36.50	54.80	72.15	1.63	3.01	0.8211	82.11
	21x10 ⁻⁶	78.89	63.60	116	46.98	1.59	3.23	0.9152	91.52



Fig. 5: Intermodulation spectrum for aluminum in 0.5 M HCl solutions without and with various concentrations of compound (2) at 25 °C



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

3.7.2. SEM Characterization

Figure 6 shows the scanning electron microphotographs of aluminum in HCl in the presence of 21×10^{-6} M of investigated compounds. As cn be seen from this Figure, there are distinct differences between the the four aluminum sheets after the corrosion in acid solution. As for bar aluminum, the surface was seriously damaged as a great deal of deep cavities and drawbach were found. Under the same corrosion circumstance, the surface of aluminum was smooth with a few small notches. The phenomenon implied that the presence of inhibitors films can protect the aluminum from corrosion efficiently. On comparing these microphotographs, it appears that maximum smoothing of the surface of test materials has been observed in presence of compound (2) followed by compound (1). This observation is in conformity with the observed inhibition efficiency values as discussed earlier.





In presence of inhibitor I In presence of inhibitor II Fig. 6: SEM photograph of aluminum for free metal, in absence of inhibitors, and presence of 21×10^{-6} M inhibitors 1 & 2

3.7 Mechanism of Corrosion Inhibition

In general, these inhibitors may be adsorbed on aluminum surface in their neutral or protonated forms (cationic form). Since it is well known that the aluminum surface is negatively charged in acid solution [60], it is easier for the protonated molecules to approach the negatively charged aluminum surface due to the electrostatic attraction. In case of adsorption, this involves the displacement of water molecules from the aluminum surface and sharing electrons between the hetero-atoms and aluminum. Also, the inhibitor molecules can absorb on aluminum surface on the basis of donor-acceptor interactions between π -electrons of aromatic rings and vacant p-orbitals of surface aluminum atoms. Thus, we can conclude that inhibition of aluminum corrosion in HCl is mainly due to electrostatic interaction. The



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

decrease in inhibition efficiency with rise in temperature (Table 7) supports electrostatic interaction. The order of decreasing inhibition efficiency of the compounds from all techniques used is: inhibitor 2 > inhibitor 1. Inhibitor 2 has the highest percentage inhibition efficiency, this being due to its larger molecular size than compound (1) which cover larger area from aluminum surface. Also, NO₂ group in compound (2) may reduce in HCl and the secondary product is the compound which adsorbed on aluminum surface.

IV.CONCLUSIONS

The investigated compounds are good inhibitors for the corrosion of aluminum in HCl solutions and they act as mixed type inhibitors. The results obtained from all the electrochemical measurements show that the inhibition properties increase with small differences in their %IE numerical values. Double layer capacitances decrease with respect to blank solution when these compounds were added. This fact may explained by adsorption of these molecules on the aluminum surface. The adsorption of the investigated chalcone derivatives on aluminum surface in HCl solution follows Langmuir adsorption isotherm. The negative values of ΔG°_{ads} show the spontaneity of the adsorption process.

REFERENCES

[1] R. Rosliza, W.B. Wan Nik, H.B. Senin, "The effect of inhibitor on the corrosion of aluminum alloys in acidic solutions", Mater. Chem. Phys., vol. 107, pp. 281-288, 2008.

[2] A. Aytac, "Cu(II), Co(II) and Ni(II) complexes of -Br and -OCH₂CH₃ substituted Schiff bases as corrosion inhibitors for aluminum in acidic media", J. Mater. Sci., vol. 45, pp. 6812-6818, 2010.

[3] I.B. Obot, N.O. Obi-Egbedi, "Fluconazole as an inhibitor for aluminium corrosion in 0.1 M HCl" Colloids Surf A: Physicochem. Eng. Asp., vol. 330, pp. 207-212, 2008.

[4] E. Foad El-Sherbini, S.M. Abd-El-Wahab, M.A. Deyab, "Studies on corrosion inhibition of aluminum in 1.0 M HCl and 1.0 M H_2SO_4 solutions by ethoxylated fatty acids" Mater. Chem. Phys., vol. 82, pp. 631-637, 2003.

[5] I. Lukovits, E Kalman, F. Zucchi, "Corrosion Inhibitors—Correlation Between Electronic Structure and Efficiency, I. Lukovits, E. Kalman, F. Zucchi Corrosion, vol. 57, pp. 3-9, 2001.

[6]] C.M.A. Brett, I.A.R. Gomes, J.P.S. Martins, "The electrochemical behaviour and corrosion of aluminium in chloride media. The effect of inhibitor anions", Corros. Sci., 36 pp. 915-923, 1994.

[7] S. Zein El Abedin, "Role of chromate, molybdate and tungstate anions on the inhibition of aluminiumin chloride solutions" J. Appl. Electrochemistry, vol. 31, pp. 711-718, 2001.

[8] S.M. Mousavifard, P.M.M. Nouri, M.M. Attar, B. Ramezanzadeh, "The effects of zinc aluminum phosphate (ZPA) and zinc aluminum polyphosphate (ZAPP) mixtures on corrosion inhibition performance of epoxy/polyamide coating", Journal of Indus-trial and Engineering Chemistry, vol. 19, pp. 1031-1039, 2013.

[9] E.M. Sherif, S.-M. Park, "Effects of 1,5-Naphthalenediol on Aluminum Corrosion as a Corrosion Inhibitor in 0.50 M NaCl" J. Electrochem. Soc. vol. 152, pp. B205-B211, 2005.

[10] P.M. Natishan, E. McCafferty, G.K. Hubler, "Surface Charge Considerations in the Pitting of Ion - Implanted Aluminum" J. Electrochem. Soc., 135, pp. 321-327, 1988.

[11] E.S.M. Sherif, "Corrosion and Corrosion Inhibition of Aluminum in Arabian Gulf Seawater and Sodium Chloride Solutions by 3-Amino-5-Mercapto-1,2,4-Triazole", Inter. J. Electrochem. Sci., vol. 6, pp. 479-1492, 2011.

[12] A.Y. El-Etre, "Inhibition of acid corrosion of aluminum using vanillin", Corros. Sci., vol. 43, pp. 1031-1039, 2001.

[13] N.A. Ogurtsov, A.A. Pud, P. Kamarchik, G.S. Shapoval, "Corrosion inhibition of aluminum alloy in chloride mediums by undoped and doped forms of polyaniline", Synthetic Metals, vol. 143, pp. 43-47, 2004.

[14] S.B. Saidman, J.B. Bessone, "Electrochemical preparation and characterisation of polypyrrole on aluminium in aqueous solution" J. Electroanal. Chem., vol. 521, (2002) 87-94.

[15] E.-S.M. Sherif, "Effects of 3-Amino-1,2,4-triazole-5-thiol on the Inhibition of Pure Aluminum Corrosion in Aerated Stagnant 3.5 wt.% NaCl Solution as a Corrosion Inhibitor" Int. J. Electrochem. Sci., vol. 7, pp. 4847-4859, 2012.

[16] E.-S.M. Sherif, A.A. Almajid, "Surface protection of copper in aerated 3.5% sodium chloride solutions by 3-amino-5-mercapto-1,2,4-triazole as a copper corrosion inhibitor", J. Appl. Electrochem., vol. 40, pp. 1555-1562, 2010.

[17] E.-S.M. Sherif, "Electrochemical and Gravimetric Study on the Corrosion and Corrosion Inhibition of Pure Copper in Sodium Chloride Solutions by Two Azole Derivatives", Inter. J. Electrochem. Sci., vol. 7, pp. 1482-1859, 2012.

[18] E.-S.M. Sherif, "Corrosion Behavior of Copper in 0.50 M Hydrochloric Acid Pickling Solutions and its Inhibition by 3-Amino-1,2,4-triazole and 3-Amino-5-mercapto-1,2,4-triazole", Inter. J. Electrochem. Sci., vol. 7, pp. 1884-1897, 2012.

[19] E.-S.M. Sherif, R.M. Erasmus, J.D. Comins, "Corrosion of copper in aerated acidic pickling solutions and its inhibition by 3-amino-1,2,4-triazole-5-thiol", Journal of Colloid and Interface Science, vol. 306, pp. 96-104, 2007.

[20] E.-S.M. Sherif, R.M. Erasmus, J.D. Comins, "Corrosion of copper in aerated synthetic sea water solutions and its inhibition by 3-amino-1,2,4-triazole", Journal of Colloid and Interface Science, vol. 309, pp. 470-477, 2007.

[21] E.-S.M. Sherif, R.M. Erasmus, J.D. Comins, "Effects of 3-amino-1,2,4-triazole on the inhibition of copper corrosion in acidic chloride solutions", Journal of Colloid and Interface Science, vol. 311, pp. 144-151, 2007.

[22] E.S.M. Sherif, R.M. Erasmus, J.D. Comins, "Inhibition of corrosion processes on copper in aerated sodium chloride solutions by 5-(3-aminophenyl)-tetrazole", J. Appl. Electrochem., vol. 39, 83-91, 2009.



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

[23] E.S.M. Sherif, R.M. Erasmus, J.D. Comins, "Inhibition of copper corrosion in acidic chloride pickling solutions by 5-(3-aminophenyl)-tetrazole as a corrosion inhibitor", Corros. Sci., vol. 50, 3439-3445, 2008.

[24] E.M. Sherif, S.-M. Park, "Effects of 2-amino-5-ethylthio-1,3,4-thiadiazole on copper corrosion as a corrosion inhibitor in aerated acidic pickling solutions", Electrochim. Acta, vol. 51, pp. 6556-6562, 2006.

[25] E.M. Sherif, S.-M. Park, "2-Amino-5-ethyl-1,3,4-thiadiazole as a corrosion inhibitor for copper in 3.0% NaCl solutions", Corros. Sci., vol. 48, pp. 4065-4079, 2006.

[26] E.-S.M. Sherif, "Effects of 2-amino-5-(ethylthio)-1,3,4-thiadiazole on copper corrosion as a corrosion inhibitor in 3% NaCl solutions", Appl. Surf. Sci., vol. 252, pp. 8615-8623, 2006.

[27] E.-S.M. Sherif, "Corrosion and Corrosion Inhibition of Pure Iron in Neutral Chloride Solutions by 1,1'-Thiocarbonyldiimidazole", International J.Electrochem. Sci., vol. 6, pp. 3077-3092, 2011.

[28] E.-S.M. Sherif, "Effects of 5-(3-Aminophenyl)-tetrazole as a Corrosion Inhibitor on the Corrosion of Mg/Mn alloy in Arabian Gulf Water" Inter. J. Electrochem. Sci., vol. 6, pp. 5372-5387, 2011.

[29] E.-S.M. Sherif, A.H. Ahmed, "Synthesizing New Hydrazone Derivatives and Studying their Effects on the Inhibition of Copper Corrosion in Sodium Chloride Solutions", Synthesis Reactivity in Inorganic, Metal-Organic, and Nano- Metal Chemistry, vol. 40, pp. 365-372, 2010.

[30] E.S.M. Sherif, "Effects of exposure time on the anodic dissolution of Monel-400 in aerated stagnant sodium chloride solutions", J. Solid State Electrochem., vol. 16, pp. 891-899, 2012.

[31] E.S.M. Sherif, "Effects of 5-(3-aminophenyl)-tetrazole on the inhibition of unalloyed iron corrosion in aerated 3.5% sodium chloride solutions as a corrosion inhibitor", Materials Chemistry and Physics, vol. 129, pp. 961-967, 2011.

[32] E.S.M. Sherif, "Corrosion Mitigation of Copper in Acidic Chloride Pickling Solutions by 2-Amino-5-ethyl-1,3,4-thiadiazole", J. Mate. Eng. Perform., vol. 19, pp. 873-879, 2010.

[33] O.L. Riggs Jr., C.C. Nathan (Ed.), Corrosion Inhibitors, 2nd ed., NACE, Houston, TX, 1973.

[34]T. Tronina, A. Bartmańska, B. Filip-Psurska, J. Wietrzyk, J. Popłoński, E. Huszcza, "Fungal metabolites of xanthohumol with potent antiproliferative activity on human cancer cell lines in vitro", Bioorganic& Medicinal Chemistry, vol. 21, pp. 2001-2006, 2013.

[35] E. E. Oguzie, "Corrosion inhibition of mild steel in hydrochloric acid solution by methylene blue dye", Mater. Letters, vol. 59, pp. 1076-1079, 2005.

[36] Gamry Echem Analyst Manual (2003).

[37] R.G. Pearson, "Absolute electronegativity and hardness: application to inorganic chemistry" Inorg. Chem., vol. 27, pp. 734-740, 1988.

[38] E. E. Ebenso, P. C. Okafor, U. J. Ekpe, "Studies on the inhibition of aluminum corrosion by 2-acetylphenothiazine in chloroacetic acids", Anti-Corrosion Methods & Materials, vol. 50, pp. 414-421, 2003.

[39] E. McCafferty, H. Leidheiser (Ed.), "Corrosion Control by Coating", Science Press, Princeton, NJ (1979) pp. 279.

[40] S.A. Umoren, E.E. Ebenso, "The synergistic effect of polyacrylamide and iodide ions on the corrosion inhibition of mild steel in H₂SO₄" Mater. Chem. Phys., vol. 106, pp. 387-393, 2007.

[41] E.E Oguzie, E.E. Ebenso, "Studies on the corrosion inhibiting effect of Congo red dye-halide mixtures", Pig. Resin Technol., vol.1, pp. 35-30 2006.

[42] R.F.V Villamil, P. Corio, J.C. Rubin, S.M.L. Agostinho, "Effect of sodium dodecylsulfate on copper corrosion in sulfuric acid media in the absence and presence of benzotriazole", J. Electroanal. Chem., vol. 472, pp. 112-119, 1999.

[43] M. Kliskic, J. Radosevic, S. Gridic, "Pyridine and its derivatives as inhibitors of aluminium corrosion in chloride solution", J. Appl. Electrochem., vol. 27, pp. 947-952, 1997.

[44] K. Aramaki, N. Hackerman, "Inhibition Mechanism of Medium - Sized olymethyleneimine", J. Electrochem. Soc., vol. 116, pp. 568-574, 1969.

[45] L. Tang, X. Li, L. Li, G. Mu, G. Liu, "The effect of 1-(2-pyridylazo)-2-naphthol on the corrosion of cold rolled steel in acid media: Part 2: Inhibitive action in 0.5 M sulfuric acid", Mater. Chem. Phys., vol. 97, pp. 301-307, 2006.

[46] F.M. Donahuce, K. Noor, "Theory of Organic Corrosion Inhibitors: Adsorption and Linear Free Energy Relationships Electron", J. Electrochem. Soc., vol. 112, pp. 886-891, 1965.

[47] P.C. Okafor, M.E. Ikpi, I.E. Uwah, E.E. Ebenso, U.J. Ekpe, S.A. Umoren, "Inhibitory action of Phyllanthus amarus extracts on the corrosion of mild steel in acidic media", Corros. Sci., vol. 50, pp. 2310-2317, 2008.

[48] Y. Ren, Y. Luo, K. Zhang, G. Zhu, X. Tan, "Lignin terpolymer for corrosion inhibition of mild steel in 10% hydrochloric acid medium" Corros. Sci., vol. 50, pp. 3147-3153, 2008.

[49] E.E. Oguzie, "Corrosion inhibition of aluminum in acidic and alkaline media by Sansevieria trifasciata extract", Corros. Sci., vol. 49, pp. 1527-1539, 2007.

[50] A.S. Fouda, A.A.Al. Sarawy, E.E.El. Katori, "Pyrazolone derivatives as corrosion inhibitors for C-steel in hydrochloric acid solution", Desalination, vol. 201, pp. 1-13, 2006.

[51] S. Martinez, M. Matkos-Hukovic, "A nonlinear kinetic model introduced for the corrosion inhibitive properties of some organic inhibitors" J. Appl. Electrochem., vol. 33, pp. 1137-1147, 2003.

[52] S.A. Umoren, I. B. Obot, E.E.Ebenso, P. C. Okafor, O.Ogbobe and E. E. Oguzie, "Gum Arabic as potential corrosion inhibitor for aluminum in alkaline medium and its adsorption characteristics", Anti-Corrosion Methods & Materials, vol. 53, pp. 277-282, 2006.

[53] J.O.M Bockris, D. Drazic, "The kinetics of deposition and dissolution of iron: Effect of alloying impurities", Electrochem. Acta, vol. 7, pp. 293-313, 1962.

[54] J. Bessone, C. Mayer, K. Tuttner, W. J. lorenz, "AC-impedance measurements on aluminium barrier type oxide films" Electrochim. Acta, vol. 28, pp. 171-175, 1983.

[55] E.A. Noor, "Evaluation of inhibitive action of some quaternary N-heterocyclic compounds on the corrosion of Al-Cu alloy in hydrochloric acid" Mater. Chem. Phys., vol. 114, pp. 533-541, 2009.

[56] I. Epelboin, M. Keddam, H. Takenouti, "Use of impedance measurements for the determination of the instant rate of metal corrosion", J. Appl. Electrochem. vol. 2, pp. 71-79, 1972.



(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 3, March 2014

[57] R.W. Bosch, J. Hubrecht, W.F. Bogaerts, B.C. Syrett, "Electrochemical Technique for Online Corrosion Monitoring", Corrosion, vol. 57, pp. 60-70, 2001.

[58] F. Bentiss, M. Bouanis, B. Mernari, M. Traisnel, H. Vezin, M. Lagrenee, "Understanding the adsorption of 4H-1,2,4-triazole derivatives on mild steel surface in molar hydrochloric acid", Appl. Surf. Sci., vol. 253, pp. 3696-3704, 2007.

[59] E. Kus, F. Mansfeld, "An evaluation of the electrochemical frequency modulation (EFM) technique", Corros. Sci., vol. 48, pp. 965-979, 2006. [60] R.K. Dinnappa, S.M. Mayanna, "Benzoic acid and substituted benzoic acids as interfacial corrosion inhibitors for copper in HClO₄", J. Appl. Elcreochem., vol. 11, pp. 111-116, 1982.