Particle Swarm Optimization Based Direct Torque Control of Brushless DC Motor

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ABSTRACT: This paper deals with the direct torque control (DTC) of BLDC motor drives by using particle swarm optimization technique. BLDC motors have wide variety of advantages like higher speed ranges, higher efficiency, and better speed versus torque characteristics. Direct torque control (DTC) is one of the efficient methods used in variable frequency drives to control the BLDC motor. DTC offers many advantages like fast torque response, no need of coordinate transformation and less dependence on the rotor parameters. In DTC, the estimated flux magnitude and torque are compared with their reference values. The reference torque is generated from the output of the speed regulator (PI controller). Tuning PI parameters (Kp, Ki) are essential to DTC system to improve the performance of the system at low speeds. In conventional PI controller, the performance of the motor may cause unexpected torque disturbances. Particle swarm optimization (PSO) is proposed to adjust the parameters (Kp, Ki) of the speed controller in order to minimize torque ripple, flux ripple, and stator current distortion. The simulation results of BLDC drive employing conventional PI and PSO based PI controllers is compared and evaluated under various load disturbances in the MATLAB/simulink environment.

KEYWORDS: BLDC motor, DTC, PI, PSO, MATLAB/simulink.

INTRODUCTION

Current researches have been tailored towards developing brushless direct current motors, which are fast becoming alternatives to the conventional dc motor types. The Brushless Direct Current (BLDC) motors are gaining grounds in the industries, especially in the areas of appliances production, aeronautics, medicine, consumer and industrial automations and so on. The BLDC motors are typically permanent magnet synchronous motors that are well driven by dc voltage. Some of the advantages of a brushless dc motor over the conventional brushed dc motors are better speed versus torque characteristics, high dynamic response and high efficiency. Another vital advantage is that the ratio of torque delivered to the size of the motor is higher, and this contributes to its usefulness in terms of space and weight consideration. There are several methods to vary the speed of a BLDC motor over a wide range. Techniques for control of current include vector control, predictive control, dead-beat control, and direct torque control. The most modern technique is direct torque control method (DTC). The DTC offers many advantages like fast torque response, no need of coordinate transformation and less dependence on the rotor parameters. The conventional PI (proportional, integral) control method is widely used in motor control system due to the simple control structure and easiness of design. However tuning the parameters of PI controller is a difficult task. To enhance the capabilities of traditional PI parameter tuning techniques, several intelligent approaches have been suggested such as genetic algorithms (GA) and the particle swarm optimization (PSO).

Particle Swarm Optimization is one of the modern algorithms used to solve global optimization problems. Thus, to solve an optimization problem, PSO applies a simplified social model. Compared to other methods, application of the PSO is simple to implement, it can quickly find a number of high quality solutions, and has stable convergence characteristics. The PSO method is an excellent optimization methodology and a promising approach for solving the optimal PI controller parameters problem.
Purpose of the present work:

The objective of the present work is to provide an alternative approach to improve the speed performance of BLDCM drive. This method uses the principle of Direct Torque Control, which is based both on field oriented control (FOC) as well as on the direct self-control theory. DTC offers direct control of stator flux and electrical torque thereby reducing the speed error resulting in better speed control of BLDC drive. In this project one of the modern algorithms called particle swarm optimization technique is used to reduce the speed error of BLDC motor, hence overcoming the major drawbacks of conventional methods.

II. MATHEMATICAL MODELING OF BLDC MOTOR

Typically, the mathematical model of a brushless DC motor is not totally different from the conventional DC motor. The major difference is the phases involved in the operation of BLDC motor drive will peculiarly affect the resistive and the inductive nature of the BLDC model arrangement. The mathematical model of the BLDC motor is modelled based on the equations illustrated below:

The coupled equations of the stator windings in terms of motor electrical constants are

\[ V_{an} = iaR + ea + L\frac{dia}{dt} \]  
\[ V_{bn} = ibR + eb + L\frac{dib}{dt} \]  
\[ V_{cn} = icR + ec + L\frac{dic}{dt} \]  

Where,

\( L \) - armature self-inductance [H]
\( V_a, V_b, V_c \) - terminal phase voltages [V]
\( R \) - armature resistance [Ω]
\( e_a, e_b, e_c \) - motor back-EMFs [V].

The electromagnetic torque is given by

\[ T_e = [e_a i_a + e_b i_b + e_c i_c] \frac{1}{\lambda_p \omega_m} \]  

The instantaneous induced emfs can be written as

\[ e_a = f_a(\theta_r) \lambda_p \omega_m \]  
\[ e_b = f_b(\theta_r) \lambda_p \omega_m \]  
\[ e_c = f_c(\theta_r) \lambda_p \omega_m \]  

Where the functions \( f_a(\theta_r), f_b(\theta_r), f_c(\theta_r) \) have same shape as induce emfs and \( \lambda_p \) is rotor magnetic flux linkage(wb).
The equation of motion for a simple system with inertia $J$, friction coefficient $B$, and load torque $T_l$ is

$$J \frac{d^2 \omega_m}{dt^2} + B \omega_m = T_e - T_l \quad (8)$$

### III. DIRECT TORQUE CONTROL OF BLDC MOTOR

DTC strategies have been widely implemented in induction machine drives. They allow a direct control of the electromagnetic torque and the stator flux through the application of suitable combinations of the control signals of the inverter switches. Therefore in DTC, Torque is controlled through the selection of optimal inverter switching states. DTC technique is superior to vector control because of the advantages like fast torque response, low inverter switching frequency, low harmonic loss, absence of coordinate transformation. This control strategy in this paper has been applied for BLDC drive.

![Fig 2: Block diagram of direct torque control of BLDC motor](image)

The basic control algorithm of DTC consists of two independent hysteresis comparators producing the error signal of stator flux and electrical torque. A two-level hysteresis flux comparator and a three level hysteresis torque comparator compare the actual values to the reference values produced by flux and torque reference controllers. Depending on the outputs from the two hysteresis controllers, the optimum switching logic selects one of the six voltage vectors and two zero voltage vectors generated by a VSI in order to keep stator flux and torque within the limits of two hysteresis bands. The angle of the stator flux vector is used to determine the voltage sector as shown on the Fig.3.

![Fig.3 Voltage vector diagram](image)
Six nonzero vectors \((V_1 \text{–} V_6)\) shape the axes of a hexagonal as depicted in the above figure and feed electric power to the load. The angle between any adjacent two non-zero vectors is 60 degrees. Meanwhile, two zero vectors \((V_0 \text{ and } V_7)\) are at the origin and apply zero voltage to the load. The eight vectors are called the basic space vectors and are denoted by \(V_0, V_1, V_2, V_3, V_5, V_6\) and \(V_7\). Assuming the stator flux vector laid on the sector I of the \(d-q\) plane, \(V_1, V_2, V_6\) could be selected to increase the stator flux vectors. Conversely, \(V_3, V_4, V_5\) could be selected to decrease the stator flux vector. The zero (null) voltage vectors does not effect on the stator flux vector. Voltage vectors are selected to control the torque also. In general, \(V_2\) and \(V_3\) vectors can be selected to increase the torque and \(V_5\) and \(V_6\) vectors will decrease the torque. Table 1 shows voltage vector selection according to stator flux and torque errors.

### Table 1: Switching Voltage Vectors

<table>
<thead>
<tr>
<th>(S_p)</th>
<th>(S_f)</th>
<th>Sector I (-30 \text{ to } 30)</th>
<th>Sector II (30 \text{ to } 90)</th>
<th>Sector III (90 \text{ to } 150)</th>
<th>Sector IV (150 \text{ to } 210)</th>
<th>Sector V (210 \text{ to } 270)</th>
<th>Sector VI (270 \text{ to } 330)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0</td>
<td>(V_2) (V_3) (V_4) (V_5) (V_6) (V_1)</td>
<td>(V_0) (V_7) (V_0) (V_7) (V_0)</td>
<td>(V_1) (V_2) (V_3) (V_4) (V_3) (V_4)</td>
<td>(V_5) (V_6) (V_1) (V_2)</td>
<td>(V_0) (V_7) (V_0) (V_7)</td>
<td>(V_0) (V_7) (V_0) (V_7)</td>
</tr>
<tr>
<td>0</td>
<td>-1</td>
<td>(V_6) (V_1) (V_2) (V_3) (V_4) (V_3) (V_4)</td>
<td>(V_7) (V_0) (V_7) (V_0)</td>
<td>(V_1) (V_2) (V_3) (V_4) (V_1) (V_2)</td>
<td>(V_5) (V_6) (V_1) (V_2)</td>
<td>(V_0) (V_7) (V_0) (V_7)</td>
<td>(V_0) (V_7) (V_0) (V_7)</td>
</tr>
<tr>
<td>-1</td>
<td>1</td>
<td>(V_5) (V_6) (V_1) (V_2) (V_3) (V_4) (V_3) (V_4)</td>
<td>(V_7) (V_0) (V_7) (V_0)</td>
<td>(V_1) (V_2) (V_3) (V_4) (V_1) (V_2)</td>
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<td>(V_0) (V_7) (V_0) (V_7)</td>
</tr>
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</table>

## IV. PARTICLE SWARM OPTIMIZATION

Particle swarm optimization is a heuristic global optimization method put forward originally by Doctor Kennedy and Eberhart in 1995. It is developed from swarm intelligence and is based on the research of bird and fish flock movement behaviour. PSO has two primary operators; velocity and position update. In this paper the main objective of PSO is minimization of speed error. Fig.4 shows the block diagram for PI controller and the corresponding objective function is as shown in equation (9) and (10).

\[
\omega_{\text{ref}}T_e^* \rightarrow K_p + K_i/S \rightarrow \omega_{\text{actual}}
\]

\[
e(t) = (\omega_{\text{ref}} - \omega_{\text{actual}}) \quad (9)
\]

\[
e(t) = T_e^*/(kp + ki)t \quad (10)
\]

Fig.4. PI controller

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PSO algorithm:

**Step.1 initialization**

Determine the particle size \( m \) and set the values of parameters \( c_1 \) and \( c_2 \).
Initialize weight factor \( w \).
Randomly generate the particles to be the candidate solutions to the optimization problem called population vector.

- Where \( m \) = particle size.

Population vector (PV) is generated by using the formula:
\[
P_{V} = k_{p_{min}} + (\text{rand}(m, 1) \times (k_{p_{max}} - k_{p_{min}})).
\]

Substitute this data in objective function to obtain fitness vector.

Fitness vector = \[ ]_{m \times 1}.

**Step.2 velocity vector calculation \( v(t) \)**

In the original version of PSO, each component of velocity vector is kept within the range \([-V_{max}, V_{max}]\).

\[ V_{max} = \frac{(k_{p_{max}} - k_{p_{min}})}{n}; \]

Where \( n \) = number of iterations.
Order of velocity vector = \( p_{s} \times n_{cv} \).
Where \( p_{s} \) = particle size,
\( n_{cv} \) = number of control variables.

**Step.3 Calculation of pbest and gbest**

pbestpopulation = population vector (pv).
pbestfitness = fitness vector (fv).

Gbest is the best position among all individual best positions achieved so far.

**Step.4 Iteration process**

Weight updating
\[ W(t) = \alpha \times w(t-1). \]
Where \( \alpha \) = random number.

Velocity updating
\[ V(t) = W(t) \times v(t-1) + c_1 \times r_1 \times (pbest-x_i) + c_2 \times r_2 \times (gbest-x_i). \]
Where \( x_i \) = current location.

Position updating
\[ X_{i,k+1} = v(t) + x_{i,k} \]
Where \( X_{i,k+1} \) = new position.
\[ X_{i,k} \] = previous location.

**Step.5 Stopping criteria**

The objective function (fitness) value is calculated for each agent according to above steps, that is \( E_{pbest} \). Compare particle’s fitness evaluation \( (E_{pbest}) \) with its Gbest. If current value is better than Gbest then set Gbest equal to the current value and that position equal to the current location \( x_i \) in D-dimensional space.

**Step.6 Exit condition**

If \( E_{pbest} < \text{error} \),

- the number of iterations reaches the maximum allowable number.

If one of the above conditions is satisfied then stop. Else go to step 4.
The optimal values of \( k_p \) and \( k_i \) are substituted in the conventional DTC and the results are obtained.

V. RESULT AND DISCUSSION

The optimized values obtained from PSO program are substituted in DTC system and the results have observed. To validate the performance of PSO based DTC different load torques has been applied as shown in fig 5(a), 6(a), 7(a),
and 8(a). The motor speed waveforms related to the PSO based DTC in comparison with conventional PI based DTC are as shown in fig 5(b), 6(b), 7(b), 8(b).

In the fig 5(b), it shows the plot of time Vs speed for a load disturbance applied to DTC of BLDC drive in fig 5(a), by comparing the speed behaviour of conventional PI based DTC with PSO based DTC of BLDC motor, there is less ripple in speed and results in better steady state response of the PSO based DTC.

In the fig 6(b), it shows the plot of time Vs speed for a load disturbance applied to DTC of BLDC drive in fig 6(a), by comparing the speed behaviour of conventional PI based DTC with PSO based DTC of BLDC motor, there is less ripple in speed and results in better steady state response of the PSO based DTC.
In the fig 7(b), it shows the plot of time Vs speed for a load disturbance applied to DTC of BLDC drive in fig.7(a), by comparing the speed behaviour of conventional PI based DTC with PSO based DTC of BLDC motor, there is less ripple in speed and results in better steady state response of the PSO based DTC.

It has been observed that the speed performance of a PSO based DTC is better when compared with the conventional DTC.

VI. CONCLUSION

In this paper, the proposed PSO based DTC of BLDC drive control scheme has been implemented. The simulation results of this method have improved the speed performance of the BLDC motor irrespective of the load torque fluctuations. The PSO method has optimized the parameters of PI controller by minimizing the speed error. It can be concluded that the PSO algorithm employed in DTC of BLDC motor has resulted in the optimal generation of kp, ki values. This method has finally improved the dynamic speed behaviour of the BLDC motor when compared with that of a Conventional PI controller based DTC of BLDC motor.

REFERENCES