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An MPI Daemon-Based Temperature Controller for an AC Susceptometer

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ABSTRACT: MPI-based daemon programmes have been employed to control temperature by varying ON/OFF time of a heater through CTC port of a microprocessor. The temperature controller daemon programme has location-wise memory - each location remembers previous integral value for heater power corresponding to it. This allows the system to gauge the correct heater power to output when the temperature controller is used for different locations with different thermal surroundings. This feature is particularly useful for the case where a sample has to be moved in an ac susceptometer.

Keywords: Temperature controller, Message Passing Interface, Daemon programmes, Pulse width modulation, location-wise memory.

I.INTRODUCTION

In order to accurately control and measure the sample temperature, a temperature controller is essential. There are many approaches control temperature like ON/OFF, Proportional (P), Proportional Derivative (PD) and Proportional Integral Derivative (PID). These control mechanisms are based on Conventional Control Logic (CCL). There is another control logic - Fuzzy Logic Control (FLC) [1] which has become very popular recently. Here we have used MPI-based-daemons-controlled programmes by CCL PID control mechanism for temperature control using a microprocessor.

II.DAEMONS

In programming parlance a daemon is a stand-alone programme running in 'userspace' (as opposed to kernel modules which run in kernel space) which handles a particular type of activity, often related to control of hardware. The *CUPS* (*Common Unix Printing System*) or *lpd* (*line printer daemon*) daemons are such examples in *linux* operating system which control the printers. This is necessary because if the printer hardware is directly accessible from the user programmes, multiple programmes trying to simultaneously access the printer will cause the lines to get jumbled up. So some form of arbitration is necessary. The *CUPS* or *lpd* daemons handle spooling, print job scheduling and checking for printer availability (if the printer is off, offline or out of paper, the daemon places the print job in a queue and tries to print it periodically.

User programmes generally 'request' the daemons to perform specific tasks. For example, the *lpr* command in UNIX does not try to access the printer hardware but instead requests the *CUPS* or *lpd* daemon to do the work. This means that programs need to communicate among themselves, a feature generally referred to as *IPC* or *Inter Process Communication*. If the two programmes run on the same computer, this communication is handled by the kernel by basically copying data between memory locations, but in the case of programmes running on different computers, networking has to be invoked.

In our setup, a number of sub-systems need to work together to make measurements possible. As an example, our 16channel meter uses hardware controlled by the Z80A microprocessor. On the other hand, the temperature controller needs to access the Z80 Counter-Timer (CTC) to change heater power through pulse-width modulation. The CTC is



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controlled by the same microprocessor (they are on the same training kit board). Now if a request for a change of CTC setting comes through while the meter is measuring something, a conflict should occur, scuttling both processes. Our solution is to have a daemon to control communication with the microprocessor. The meter programme and temperature controller programme both send their requests to this daemon. The daemon puts the second request on hold, services the first, and handles the second one in its turn. Again, different free-running programmes may need to access different channels of the 16-channel voltmeter. This necessitates the intervention of another daemon to handle these conflicting requests. Thus two daemon programmes cascade together to allow different subsystems to work in a free-running manner. In principle it would be possible to incorporate all the steps in the measurement within the ambit of one master programme, thus eliminating the free-running nature of the different parts and hence automatically synchronising them. Then we would not need these daemons. However, the complexity of such a master programme would be huge almost to the point of being unmanageable. Multiple users would also not be able to use the system simultaneously.

III. EXPERIMENTAL DETAILS

The whole setup is divided in two parts; hardware and software. Each part is discussed as follows:

A. Hardware

The microprocessor based system used here comprises a Microprocessor trainer kit with the 4MHz *Zilog Z80A* processor [2], built-in Counter/Timer CTC, a control circuit for the heater current, computer controlled MPI-based voltmeter [3], a small heater coil made of constantan and a preamplifier circuit for sensing voltage from PT100 RTD (Resistance Temperature Detector) output.

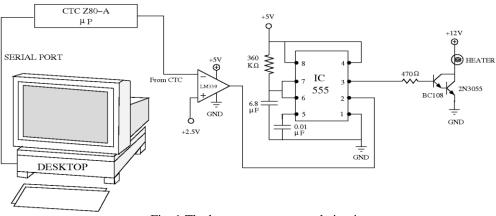


Fig. 1 The heater current control circuit.

Control circuit for heater: The pulse width modulated (PWM) heater current control circuit is shown in figure 1. Basically this circuit is controlled by the Counter/Timer circuit (CTC) of the *Z*-80 based microprocessor kit followed by a monostable multivibrator and a darlington pair. The CTC has four independent counter/timer circuits, each containing the logic as shown in figure 2.



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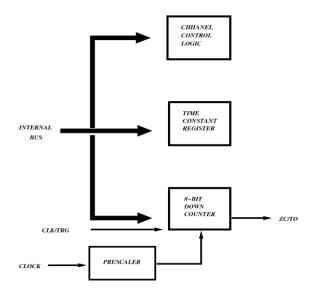


Fig. 2 Counter/timer block diagram.

The channel control logic receives 8-bit channel control word when the counter/timer channel is programmed. The channel control logic decodes the channel control word and sets the following operating conditions:

Interrupt enable (or disable).

Operating mode (Timer/counter).

Timer mode prescaler factor (16/256).

Active slope for CLK/TRG input.

Timer mode trigger (automatic or CLK/TRG input).

Time constant data word to follow.

Software reset.

Each channel of the CTC is individually programmed with two words; a control word and a time-constant word. The control word selects the operating mode (counter or timer) and other operation parameters. If the timer mode is selected, the control word sets a prescaler, which divides the system clock by either 16 or 256. The time-constant word

is a value from 1 to 256. The timer mode determines time intervals as small as $4\mu s$ (frequency 4MHz) without additional logic or software timing loops. Time intervals are generated by dividing the system clock with a prescaler (16 or 256) that decrements a preset down counter. A timer is triggered automatically when its time constant value is programmed, or by an external CLK/TRG input. In our case we have cascaded two channels of the timer/counter to make it a 'large timer'. First the timer mode is selected through control word which is followed by a time constant which is determined by the heater power controlling software. After predefined time period the output of the timer resets to zero which triggers the counter that is also operated through a control word followed by a value. This value is also calculated by the software to control the exact heater current. The control word for selecting timer mode and the counter mode is shown below:



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	Control word for timer mode								Control word for counter mode						
\mathbf{D}_7	D_6	D_5	D_4	D_3	D_2	D_1	D_0	D_7	D_6	D_5	D_4	D_3	D_2	D_1	\mathbf{D}_0
0	0	1	0	0	1	0	1	0	1	1	0	0	1	0	1
$(25)_{16}$									(65) ₁₆						

The output of the cascaded timer/counter is taken as the trigger of an IC 555 timer-based monostable multivibrator. Since the on-time of the monostable multivibrator in fixed, by varying the time constant of the timer and hence the triggering interval, the duty cycle (on-time/total time period) of the heater can be controlled. Depending on the requirement of heater power, which is calculated with the help a software by sensing the temperature by a PT100 RTD, heater current is adjusted through a darlington pair (BC108 & 2N3055) which is driven by the output of the monostable multivibrator. The heater is connected to the collector of the power transistor 2N3055. We have chosen *constantan* wire as the heating element of resistance ~ 14Ω . The wire is first insulated with Teflon tape and it is wound non-inductively like a bobbin to make it shaped like a spiral disk. The size of our heater is almost the same as that of the sample and it is mounted on one face of the sample. On the other face a Pt-100 (Platinum Resistance Thermometer) thin film type temperature sensor is attached. The voltage source of the heater as shown in figure 1 is +12V dc, but the dc source voltage can be be selected to different voltages upto +30V, if necessary.

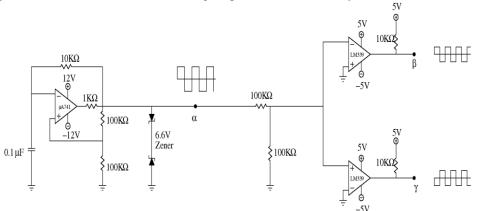


Fig. 3 Square-wave generator for temperature controller.

Temperature sensor circuit:

The circuit diagram for the temperature sensor is shown in figure 2 and 3. The main element of this circuit is a PT100 (PRT) which offers an excellent accuracy over a wide temperature range (from -200 to +850° C). Standard Sensors are available from many manufacturers with various accuracy specifications and numerous packaging options to suit most applications. The principle of operation is to measure the resistance of a platinum element. The PT100 has a resistance of 100 Ω at 0°C and 138.4 Ω at 100°C. The relationship between temperature and resistance is approximately linear over a small temperature range. The relation between the resistance and the temperature is given below:

$$R_{t} = R_{0}(1 + \alpha t + \beta t^{2} + \gamma (t - 100) t^{3}), \text{ where}$$

$$R_{t} = \text{Resistance at } 0^{\circ}\text{C}$$

$$R_{0} = \text{Resistance at } 0^{\circ}C = 100\Omega$$

$$\alpha = 3.9083 \times 10^{-3}$$

$$\beta = -5.775 \times 10^{-7}$$

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 $\gamma = -4.183 \times 10^{-12} \text{ below } (0^{\circ} C)$ or $\gamma = 0$ (above $0^{\circ}C$)

For a PT100 sensor, a 1°C temperature change will cause a 0.384Ω change in resistance, so even a small error in measurement of the resistance (for example, due to the resistance of the wires leading to the sensor) can cause a large error in the measurement of the temperature. For high precision we have followed the four-probe method where four wires are used - two to carry the sense current, and two to measure the voltage across the sensor. The current through the sensor will cause some heating. If the sensor element is unable to dissipate this heat, it will reflect as a higher temperature. To eliminate this effect we have used very small ac constant current $\approx 49\mu$ A through the sensor. A chopper amplifier is used to amplify the output signal of the PT100 to such a value that the voltmeter used here can read the voltage at better accuracy. Because of the low signal levels, the cables are kept away from electric cables, motors and other devices that may emit electrical noise.

Figure 3 shows the square-wave generator part of the temperature controller circuit. Here an op-amp based astable multivibrator is used to generate square-wave. In order to get output pulses of equal on-off time, the saturation voltage is clipped to $\pm 6.6V$ by two zeners (α). After reducing the peak voltages of the square wave it is fed to two LM339 comparators, which produce two out-of-phase square waves. The peak of the square waves are at $\pm 5V$ (β) and $\mp 5V$ (γ) with errors of $\sim 0.2V$ due to the saturation drop of the open-collectors stages. These square waves are used to control two CMOS (CD4066) switches, the outputs of which are shorted into one and inputs are connected to +5V and -5V respectively (figure 4). Thus the amplitudes of the output waveform are accurately tied to $\pm 5V$, which is maintained by accurate voltage regulator ICs. The constant current is maintained by the input resistance (100KQ) of the inverting amplifier configured as a voltage-to-current converter. The voltage across of the PT100 which is connected as the feedback resistance of the inverting amplifier, is fed through an instrumentation amplifier of 100 gain. Another pair of CMOS switches, driven by the same input signals β and γ , are now used to rectify the signal (like a LIA) and the final outputs filtered by a RC stage before being fed to the input of the 16-channel voltmeter.

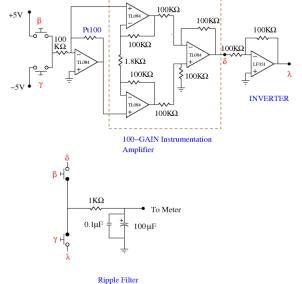


Fig. 4 Preamplifier for the temperature controller.



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B. Software:

We have introduced here MPI-based daemon programmes written in C++ and tcl/tk languages to control the heater current with the hardware. The communication model used in this work has been discussed below:

We have tried to keep scope for improvements and expansion open. Thus, from the very beginning, we have tried to allow different subsystems to run on different computers if necessary. In order to do so, we have used the free LAM (Local Area Multicomputer) software, which implements the MPI (Message Passing Interface) standard, allowing parallel programmes to run on clusters.

The main daemon program is "tempetld" (Temperature controller daemon) which controls the whole process. There is another helper program which sends requests (wake-up call) to the daemon program periodically. The daemon program senses temperature, calculates heater power and sends requests to the microprocessor CTC to feed desired pulses for maintaining heater temperature. The graphics frontend of "tempetld" is shown in figure 5. The working principle is as given below:

- It initially sets "heater power", "set temperature", "proportional term (P)", "integral term (I)" and "derivative term (D)" to 'ZERO'.
- Sends request to meter daemon (using channel 14) to measure the output of the temperature controller circuit.
- Calculates the resistance value of PT100 and displays the "Actual temperature".
- The daemon has different input variables i.e. Set Temperature; P, I, D; Modes Set / Sweep; Heater range-Low / Medium / High; Locations (6 locations). Any new entry can be made by directly inserting the values into the GUI or using a command-line program named "tempctld_set". A library of subroutines enables other programmes to send requests to "tempctld".
- After getting new values, the daemon program first calculates the required heater power using PID algorithm.
- The daemon has three heater power ranges each of which has predefined integer values.
- Depending upon the range of the heater power, the program calculates the second integer value using heater power formula.
- The daemon program sends request to microprocessor and dumps the calculated integers to the CTC.
- The CTC sends pulses with desired ON/OFF ratio to the control circuit for heater.
- The daemon now enters a blocking receive mode and waits till it is woken up either by the helper (to update the controller parameters periodically) or by some other program requesting specific actions, like changing PID or setting a new temperature, etc.
- The temperature controller can be used in two modes; set mode and sweep mode. In set mode the daemon program sets the "set temperature" and waits for any call and in the sweep mode the program starts from the initial temperature and continually changes the target temperature with a temperature rate defined by the user or any other program.
- The temperature controller daemon has six locations. The previous integral value is stored in a 6-member array. This function is very useful for controlling temperature at different positions by using a suitable starting heater power if needed.



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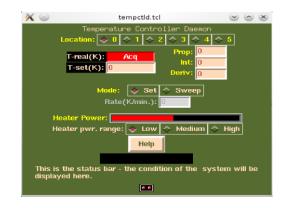


Fig. 5 Frontend for the temperature controller daemon programme.

IV. RESULTS AND DISCUSSION

The temperature controller is calibrated with DMM Mastech Model: MAS838H with temperature sensing probe. The calibration is done for $0^{\circ}C$, $100^{\circ}C$, and room temperature. The temperature controller can resolve temperature difference better than 0.2K. The location-wise setting of the daemon is very useful for such system for which sample with the temperature controller has to be moved measurements.

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