

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 2, February 2015

Simulation and Analysis of Adaptive Control Method Employed for Matrix Converter

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ABSTRACT: Since discovered, electrical energy became one of the world's fastest growing energy technologies. Efficient and stable utilization of electrical energy is one of the most important problem. The major phenomena that effects on the quality of power supply is the harmonics caused by different loads connected to the grid, which are usually converters based on power electronic components. These are the main causes for the deterioration of power quality. This paper presents the harmonic compensation of linear loads fed by matrix converter and the performance of two types of controllers(namely, Adaptive Fuzzy control and Adaptive Neural Fuzzy Inference system) are compared, during balanced supply and abnormal grid conditions. The sinusoidal nature of output currents were preserved by using PWM method and optimum Venturini method employed for matrix converter.

KEYWORDS: Matrix converter, Balanced and Unbalanced grid, Adaptive fuzzy control, ANFIS controller, Venturini modulation, Linear load, THD.

I. INTRODUCTION

The control and transformation of electrical energy is the most important process in electrical engineering. Due to the advancements of power electronics in recent years ,this work has been done by using power semiconductors and energy storage elements such as capacitors and inductors. Their response is instantaneous and automatically adapts to the changes during abnormal conditions. The increased complexity of their control and usage of more number of elements leads to the discovery of new type of converter called matrix converter which is very simple and compact. A Matrix Converter is an array of semi-conductor controlled switches used for convert the magnitude as well as the frequency of the input to a desired magnitude and frequency of the output. Basically a matrix converter consists of nine bi-directional switches, which are required to be commutated in the right way and sequence in order to minimize losses and produce the desired output waveforms with high quality. The Factors such as the absence of bulky electrolytic capacitors, reduction in size and weight of the converter, increasing power density, and obtaining almost sinusoidal nature of output wave forms are the most important characteristics of matrix converter. This paper presents the adaptive control techniques for the performance improvement of matrix converter along with Optimum Amplitude Venturini Modulation to get maximum voltage transfer ratio and to enhance the overall system stability.

II. LITERATURE SURVEY

After the controlled rectifiers were developed in the early 1930's, it was realized that this provided the possibility of generating alternating currents of variable frequency directly from a fixed frequency AC supply, the positive rectifier supplying the positive half cycles of current and the negative rectifier the negative half cycles. The first study of direct AC/AC frequency converters was presented in 1976 by Gyugyi and Pelly. In general, the conversion of an input AC power at a given frequency to an output AC power at a different frequency is called AC/AC power frequency converters can be divided in to two main categories. The first type called indirect AC/DC/AC power frequency converter consists of two or more stages of conversion with an intermediate DC link. The second type called direct AC/AC power frequency converter is a single stage power converter which consists of an



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array of semiconductor switches connected directly between the input and output terminals. The most common topology for an indirect AC/AC converter is the use of diode bridge rectifier at the supply side and a pulse width modulated voltage source inverter (PWM-VSI) at the load side .This converter consists of two power conversion stages and an intermediate energy storage element. In the first stage the input AC power is converted to uncontrolled DC power by the diode bridge rectifier. The converted DC power is then stored in DC link capacitor. In the second stage a PWM-VSI operating at a high switching frequency generates AC signals with arbitrary amplitude and frequency. Although this type of AC/AC converter is very cost-effective and reliable, it has lots of drawbacks. Due to the uncontrolled operation of diode bridge rectifier, the input AC currents drawn by the rectifier contain a large amount of harmonics that produces distortion of the input line voltages, having a negative impact on the performance of sensitive loads and equipment connected to the same supply.

The other topology called matrix converter for 3 AC/AC power converter replaces the diode bridge with PWM rectifier resulting in a back-to-back converter .This converter overcomes the input harmonic problem of the former topology and offers improved total input power factor and bi-directional power flow. The matrix converter was firstly introduced in the year 1976 by Venturini and Alesina with their intensive research on MC's and they proposed a generalised high-frequency switching strategy with huge mathematical background in 1980.They have represented the power circuit of the converter as a matrix. The main theme of this control strategy is to design an ideal electronic transformer which is capable of varying the current, voltage, power factor and frequency. [1]



II. THE BASIC TOPOLGY AND MODELLING OF MATRIX CONVERTER

Fig. 1 Basic circuit of a Matrix Converter

The matrix converter, shown in Fig. 1, is the most important from a practical point of view because it connects a threephase source to a three-phase load. The electrical power from source to load is controlled by power and control circuit of matrix converter. The input supply is connected to the matrix converter through input filter which is usually needed to smoothen the input currents, by reducing the harmonic components and it eliminates the over voltages produced due to the presence of short-circuit reactance of any real power supply at the time of commutation of currents. The bidirectional semiconductor switches are composed of two IGBT's and two fast diodes connected in anti-parallel. In order to obtain maximum voltage transformation ratio, gate signals are used to driven the bidirectional switches by using optimum amplitude venturini method. The matrix converter is a single-stage converter with $m \times n$ bidirectional semiconductor power switches that mainly connects each *m*-phase voltage source to an *n*-phase load. In this paper 3×3 matrix converter is used[1],[2].



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A. Modelling of the Matrix Converter

The input source voltage of matrix converter is given by:

$$V_{i}(t) = \begin{bmatrix} V_{AN}(t) \\ V_{BN}(t) \\ V_{CN}(t) \end{bmatrix} = V_{im} \begin{bmatrix} \cos(\omega_{i}t) \\ \cos(\omega_{i}t - \frac{2\pi}{3}) \\ \cos(\omega_{i}t - \frac{4\pi}{3}) \end{bmatrix}$$
(1)

The input line current amplitude i_{im} and phase φ_i of matrix converter is given by:

$$I_{i}(t) = \begin{bmatrix} I_{A}(t) \\ I_{B}(t) \\ I_{C}(t) \end{bmatrix} = I_{im} \begin{bmatrix} \cos(\omega_{i}t + \varphi_{i}) \\ \cos(\omega_{i}t - \frac{2\pi}{3} + \varphi_{i}) \\ \cos(\omega_{i}t - \frac{4\pi}{3} + \varphi_{i}) \end{bmatrix}$$
(2)

The most efficient approach to obtain desired output voltage and currents are determined respectively by following equations: .

$$V_{j}(t) = \begin{bmatrix} V_{aN}(t) \\ V_{bN}(t) \\ V_{cN}(t) \end{bmatrix} = V_{om} \begin{bmatrix} \cos(\omega_{o}t) \\ \cos(\omega_{o}t - \frac{2\pi}{3}) \\ \cos(\omega_{o}t - \frac{4\pi}{3}) \end{bmatrix}$$
(3)

$$I_{j}(t) = \begin{bmatrix} I_{a}(t) \\ I_{b}(t) \\ I_{c}(t) \end{bmatrix} = I_{om} \begin{bmatrix} \cos(\omega_{o}t + \varphi_{o}) \\ \cos(\omega_{o}t - \frac{2\pi}{3} + \varphi_{o} \\ \cos(\omega_{o}t - \frac{4\pi}{3} + \varphi_{o}) \end{bmatrix}$$
(4)

The nine ideal semiconductor switches of this converter are represented by S_{ij} and are characterised a connection function $S_{ii}(t)$ defined by the following equations:

$$S_{ij}(t) = \begin{cases} 0 & if S_{ij} & open \\ 1 & if S_{ij} & closed \end{cases}$$
(5)

 $S_{Aj} + S_{Bj} + S_{Cj} = 1$, where i = A, B, C and j = a, b, cThe generation function $m_{ij}(t)$ of the nine bidirectional switches S_{ij} as the average value of the connection function $S_{ij}(t)$ over a period of switching T_P are defined as follows:

$$m_{ij}(t) = \frac{1}{T_p} \int_0^T S_{ij}(t) dt \quad with \ 0 < m_{ij}(t) > 1$$
(6)

The matrix converter is fed by voltage source, so in order to prevent the short-circuit on the input side and to provide uninterrupted current flow, input terminals should not be short circuited and the output phase must never be opened .For this reason the duty cycles must satisfy the following constraints.

$$m_{Aa}(t) + m_{Ba}(t) + m_{Ca}(t) = 1$$

$$m_{Ab}(t) + m_{Bb}(t) + m_{Cb}(t) = 1$$

$$m_{Ac}(t) + m_{Bc}(t) + m_{Cc}(t) = 1$$
(7)

All the generation functions form a matrix called modulation matrix M (t) as:

$$M(t) = \begin{bmatrix} m_{Aa} & m_{Ba} & m_{Ca} \\ m_{Ab} & m_{Bb} & m_{Cb} \\ m_{Ac} & m_{Bc} & m_{Cc} \end{bmatrix}$$
(8)

The conversion matrix of matrix converter connects the electrical as follows:

$$V_{j}(t) = M(t) \cdot V_{i}(t)$$
(9)
$$V_{i}(t) = M(t)^{T} V(t)$$
(10)

$$I_i(t) = M(t)^I \cdot I_j(t) \tag{10}$$

Where, M(t) and $M(t)^T$ are modulation matrix and its transposed.



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B. PWM with three intervals using Optimum Venturini Control



Fig. 2 Simulink model of matrix converter to generate duty cycle for three output phases

In order to obtain maximum output voltage, it is necessary to add third harmonic frequency component of the input and output frequencies to the initial approach of Venturini method as shown in fig. 2, which indicates the following equations. This is called Optimum Amplitude Venturini method [2],[3],[4].

$$\begin{cases} V_{aN}(t) = qV_{im}(\cos(\omega_o t) - \frac{1}{6}\cos(3\omega_o t) + \frac{1}{2\sqrt{3}}\cos(3\omega_i t)) \\ V_{bN}(t) = qV_{im}(\cos\left(\omega_o t + \frac{2\pi}{3}\right) - \frac{1}{6}\cos(3\omega_o t) + \frac{1}{2\sqrt{3}}\cos(3\omega_i t)) \\ V_{cN}(t) = qv_{im}(\cos\left(\omega_o t + \frac{4\pi}{3}\right) - \frac{1}{6}\cos(3\omega_o t) + \frac{1}{2\sqrt{3}}\cos(3\omega_i t)) \end{cases}$$
(11)

The modulation rate (q) is the ratio between the maximum amplitude of the output voltage (V_{jm}) and the maximum amplitude of the input voltage (V_{im}) and it can be raised to 0.866 against the maximum value of 0.5 by injecting third harmonic output frequency component to the output voltages which can be determined by the following equation (12).

$$q = \frac{(v_{jm})}{(v_{im})}$$
 with $0 < q \ge 0.866$ (12)

Similarly, the modulation function according to the optimal amplitude in expression of Venturini is:

$$m_{ij}(t) = \frac{1}{3} \begin{cases} 1 + \frac{2V_i V_j}{V_{im}^2} + \frac{4q}{3.\sqrt{3}} \sin(\omega_i t) \sin(3\omega_i t) \\ 1 + \frac{2V_i V_j}{V_{im}^2} + \frac{4q}{3.\sqrt{3}} \sin(\omega_i t + \frac{2\pi}{3}) \sin(3\omega_i t) \\ + \frac{2V_i V_j}{V_{im}^2} + \frac{4q}{3.\sqrt{3}} \sin(\omega_i t + \frac{4\pi}{3}) \sin(3\omega_i t) \end{cases}$$
(13)

By using the following equation the switching time were calculated :

$$m_{ij}(t) = \frac{t_{ij}(t)}{T_p} \tag{14}$$

The carrier signal is tooth expressed by:

$$u_p(t) = \frac{1}{T_p}t \qquad 0 \le t \ge T_p \tag{15}$$

Pulse Width Modulation is used to divide the time period T_p into three intervals. It is defined with equations (14) and (15)



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Fig. 3 Obtaining turn-on-time of the switches

The fig. 3 represents the turn-on time of the bidirectional switches for one output phase. The controls of switches S_{ij} of Matrix converter are obtained using a simple logic binary:

$$X = t_{Aj}$$

$$Y = t_{Aj} + t_{Bj}$$

$$I$$

$$S_{Aj} = X_{j}$$

$$S_{Bj} = \overline{X}_{j} \text{ and } Y_{j}$$

$$S_{Cj} = \overline{X}_{j} \text{ and } \overline{Y}_{j}$$
(16)

III. DESIGNING OF CONTROLLERS

A. Adaptive Fuzzy control of a matrix converter



Fig. 4 Schema of adaptive fuzzy controller

The output current measurements of the linear RL load using adaptive fuzzy controller as given in Fig. 4.[5]. The load current and it's reference output load current are measured the according to the following equation:[6]

$$I = \sqrt{\frac{2}{3} \left(I_{N'a}^2(t) + I_{N'b}^2(t) + I_{N'c}^2(t) \right)}$$
(17)

$$I_{ref} = \sqrt{\frac{2}{3}} \left(I_{N'aref}^{2}(t) + I_{N'bref}^{2}(t) + I_{N'cref}^{2}(t) \right)$$
(18)

The output of the fuzzy controller continuously regulates the parameters of the PI controller using the error signal and its derivative at all operating conditions. Finally the fuzzy adaptive controller gives the desired voltage transformation ratio value " \mathbf{q} ". The fuzzy rules of inference of input and output variables are shown in the following table:

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e/de	NB	NM	NS	ZE	PS	PM	PB
NB	NB	NB	NM	NM	NS	NS	ZE
NM	NB	NM	NM	NS	NS	ZE	PS
NS	NM	NM	NS	NS	ZE	PS	PS
ZE	NM	NS	NS	ZE	PS	PS	PM
PS	NS	NS	ZE	PS	PS	PM	PM
PM	NS	ZE	PS	PS	PM	PM	PB
PB	ZE	PS	PS	PM	PM	PB	PB

Table 1: Fuzzy rules of inference

B. Adaptive Neural Fuzzy Inference System (ANFIS) of a matrix converter

The ANFIS controller is combined with the inference systems fuzzy logic and artificial neural network. Artificial neural network can be trained online or offline learning process. The ANFIS structure is composed of five functional blocks namely rule base, database, decision making unit, fuzzification and defuzzification interface. The ANFIS controller inputs are error from the measured load and reference currents and the derivative of error. The error signals are multiplied by their respective weights and mapped through fuzzy logic membership functions. Training the ANFIS system is actually tuning the weights to get desired value of " \mathbf{q} ".



Fig. 5 ANFIS structure layers and rules formation

The rules of the ANFIS structure are shown in Fig.5. The output of the ANFIS controller generates the required voltage ratio according to the changes in input and the duty cycles are generated according to it.

IV. SIMULAITON RESULTS

The adaptive fuzzy and ANFIS controllers are connected to the matrix converter and a set of simulations have been performed. And a comparison is made between adaptive fuzzy controller and ANFIS controller. Bidirectional switches IGBT are considered and ode23tb simulation solver was used .

A. Balanced Grid Case

Below figures show the source voltage feeds the linear load and its linear load currents using adaptive fuzzy controller for balanced grid voltage.



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Figure 6 represents the input voltage of 311V supplying linear load without any disturbances which indicates that the supply is free from harmonics and its total harmonic distortion is 0.00%



Whereas Figure 7 represents the load currents of three output phases for linear RL load when matrix converter is connected to adaptive fuzzy controller under balanced grid conditions.



Fig. 8 Harmonic spectrum analysis of linear load current (Adaptive fuzzy controller)

Figure 8 represents the harmonic content of 3.44% present in the output current waveform by using adaptivefuzzy controller without any disturbances in the supply.



The above figure 9 shows the linear load currents of RL load for three output phases when the matrix converter is controlled by ANFIS controller when the supply is balanced.



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Fig. 10 Harmonic spectrum analysis of linear load current (ANFIS controller)

From the Figure 10 which represents the THD of 3.24% for linear load currents indicates that ANFIS controller gives better results than adaptive fuzzy controller.

B. Unbalanced Grid Case



The abnormal grid voltages are applied to the matrix converter by injecting 20% third and 10% fifth harmonic with THD of 22.36%. Figure 11 represents the distortion in source voltage and in practical these disturbances are occurred due to sudden load variations, faults in the power system network and electronic goods etc.



Even though the input voltage is disturbed the adaptive fuzzy controller still maintains the sinusoidal nature of load currents which is represented in the Figure 12.



Fig. 13 Harmonic spectrum analysis of load current for unbalanced grid case (Adaptive fuzzy controller)



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The above figure shows the harmonic content of 7.99% for linear load current when the matrix converter is fed through adaptive fuzzy controller.



Figure 14 represents the linear load currents of RL load for three output phases when the matrix converter is fed through ANFIS controller when the supply is disturbed.



Fig. 15 Harmonic spectrum analysis of load current for unbalanced grid case (ANFIS controller)

The above figure shows that 7.40% of harmonics are present in the output currents using ANFIS controller. The above simulation results obtained in all the cases for RL load shows that the sinusoidal nature of linear load currents are preserved in any condition and the ANFIS controller continuously adjusts to both normal and abnormal conditions much better than adaptive fuzzy controller. At the same time ANFIS controller shows the better performance in suppressing the harmonics of linear load currents in terms of THD, which is compared with the adaptive fuzzy control in the below table[8].

Table 2: Co	omnarison	table between	Adaptive Fr	izzy and ANFIS	controllers in	terms of THD
Table 2. Co	Jinparison	table between	maphie re	ally and mining	controners m	will of the

	Input	Linear Load current(THD)		
	Voltage(THD)	Adaptive Fuzzy Controller	ANFIS controller	
Balanced Grid Case	0.00%	3.44%	3.24%	
Unbalanced Grid Case	22.36%	7.99%	7.40%	



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V. CONCLUSION

In this paper in order to evaluate the effectiveness of the results two types of controllers adaptive fuzzy controller and ANFIS controllers were used along with different cases of harmonic disturbances. The above results clearly shows that the ANFIS controller gives better results than adaptive fuzzy control and it preserves the sinusoidal nature of linear load currents. The Matrix converter along with the ANFIS controller can also be used for different loads and by further improvements it can be used in various applications like aircrafts, wind generating stations and induction motors.

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APPENDIX SYSTEM PARAMETERS:

Input voltage phase to neuter RMS: $V_i=220V$ Input frequency $f_i=50 Hz$ Input filter: $R_f = 0.8\Omega$, $L_f = 0.5mH$, $C_f = 80\mu F$. Switching frequency: $f_s=5 kHz$ Linear Load: $R_l = 10\Omega$, $L_l = 30mH$.