



# **Analysis, Simulation of 3-Stage Cockcroft-Walton Voltage Multiplier for High Step-Up Dc-Dc Converter**

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**ABSTRACT:** This paper presents a high step-up dc-dc converter based on the Cockcroft-Walton (CW) voltage multiplier without using step-up transformer. The proposed converter is quite suitable for applying low-input dc voltage, to high output dc voltage dc generation systems. It provides continuous input current to load with low ripple voltage and current. Voltage stress on the all switching device, diodes, and capacitors are lower than the other type. Moreover, based on the 3-stage Cockcroft-Walton (CW) voltage multiplier, the proposed converter can provide a suitable dc source is solar cells, fuel cell and other type source for a 3-stage multilevel inverter. In this paper, the control strategy employs two independent frequencies, one operates at high frequency to minimize the size of the inductor and other one operates at relatively low frequency to the desired output voltage ripple. The simulation is carried over by the MATLAB-SIMULINK.

**KEYWORDS:** Cockcroft-Walton (CW) voltage multiplier.

## **1.INTRODUCTION**

In generally to get high dc output voltage we are using voltage multipliers, DC-AC-DC inverters With step-up transformer due to using of transformers the size, cost and high ripples are present in output voltage and current. The Cockcroft-Walton (CW) generator, or multiplier, which is an electronic circuit it generates a high DC voltage from a low level input voltage AC or pulsing DC. Today Cockcroft-Walton (CW) circuits are still used in particle accelerators, and also in many electronic devices where high voltages require. The Applications are x-ray machines, television, and photocopiers. It is made up of ladder network of capacitors and diodes to generate high DC voltages. Here we are using only capacitors and diodes, these voltage multipliers can step up relatively low voltages to extremely high voltage, while at the same time lighter and cheaper than using step-up transformers. The biggest advantage of such circuits is that the voltage across each stage of the cascade is equal to only twice the peak input voltage in a half wave rectifier. It has the advantage of requiring relatively low cost components and easy to insulate. Possibility of taking output from any stage, like a multi tapped transformer.

**LITERATURE SURVEY:** Review of nonisolated high-step-up dc/dc converters in photovoltaic grid-connected applications,” by W. Li and X. He, *IEEE Trans. Ind. Electron.*, vol. 58, no. 4, pp. 1239–1250, Apr. 2011.

How to achieve high-step-up, low-cost, and high-efficiency dc/dc conversion is the major consideration due to the low PV output voltage with the parallel-connected structure. Providing continuous input current with low ripple, high voltage ratio and low voltage stress on the switches, diodes and capacitors.

Cascaded dc-dc converter connection of photovoltaic modules,” by G. R. Walker and P. C. Sernia, *IEEE Trans. Power Electron.*, vol. 19, no. 4, pp. 1130–1139, Jul. 2004.

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Presents New residential scale photovoltaic (PV) arrays are commonly connected to the grid by a single DC-AC inverter connected to a series string of PV modules, or many small DC-AC inverters which connect one or two modules directly to the AC grid.

## II. PROPOSED CIRCUIT

In this paper, proposed converter supplied by a low-level dc source, such as battery, PV module, or fuel cells. The proposed converter (Cockcroft–Walton (CW) generator, or multiplier) consists of one inductor  $L_s$  (boost inductor), four switches ( $S_{m1}$ ,  $S_{m2}$ ,  $S_{c1}$ , and  $S_{c2}$ ) the rating of all switches are same as well as voltage stress across each switches are same, and one n-stage CW voltage multiplier. The four switches are divided into two groups  $S_{m1}$  ( $S_{c1}$ ) and  $S_{m2}$  ( $S_{c2}$ ) which operate in complementary mode, and they are operating under two different frequencies of  $S_{m1}$  and  $S_{c1}$  are defined as  $f_{sm}$  and  $f_{sc}$ , respectively. For convenience,  $f_{sm}$  is denoted as modulation frequency, and  $f_{sc}$  is denoted as alternating frequency. The both  $f_{sm}$  and  $f_{sc}$  frequencies should be as high as possible so that we can use smaller inductor and capacitors in this circuit. In this paper,  $f_{sm}$  (=60 kHz) is set much higher than  $f_{sc}$  (=1 kHz), and the output voltage is regulated by controlling by the duty cycle of  $S_{m1}$  and  $S_{m2}$ , while the output voltage ripple can be adjusted by  $f_{sc}$ . As shown in Fig.1, the well-known CW voltage multiplier is constructed by a cascade of stages with each stage containing six capacitors ( $C_1, C_2, C_3, C_4, C_5, C_6$ ) and six diodes ( $D_1, D_2, D_3, D_4, D_5, D_6$ ). In an n-stage CW voltage multiplier, there are  $N$  ( $= 2n$ ) capacitors and  $N$  diodes  $n=3$  (3-stage).

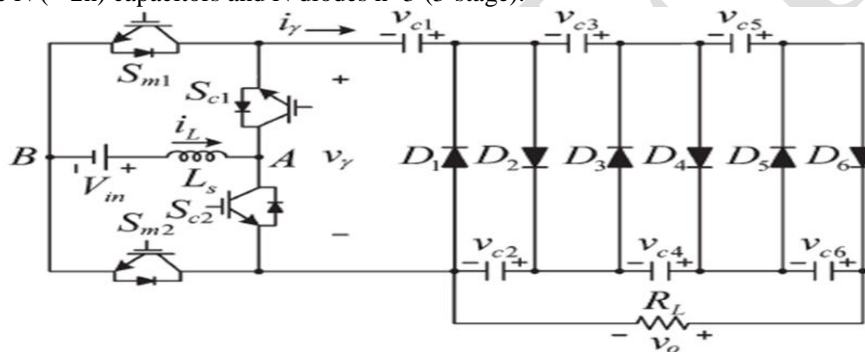
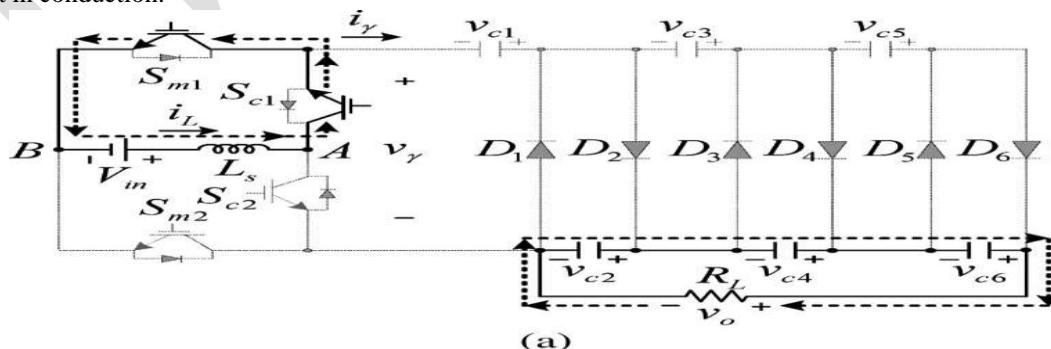


Fig. 1 3-Stage Cockcroft-Walton voltage multiplier.

## III. OPERATION

The operation of 3-stage Cockcroft-Walton (CW) Voltage Multiplier is divided to four mode operation is explained by the given below circuit diagrams from Fig. a to Fig. h

**Mode 1:**  $S_{m1}$  and  $S_{c1}$  Switches are turned on, and  $S_{m2}$ ,  $S_{c2}$  Switches turn off, and all diodes are turned off, as shown in Fig a. The boost inductor is get charged by the  $V_{in}$  which is may be fuel cell solar cell or other source, the even group capacitors  $C_6, C_4$ , and  $C_2$  are discharged and give supply to the load, the odd-group capacitors  $C_5, C_3$ , and  $C_1$  are not in conduction.

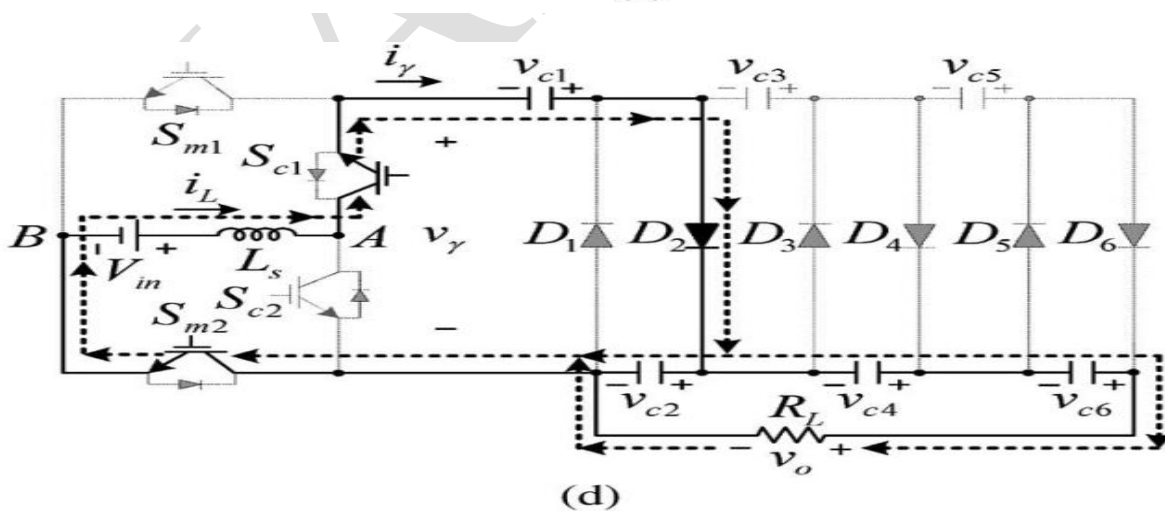
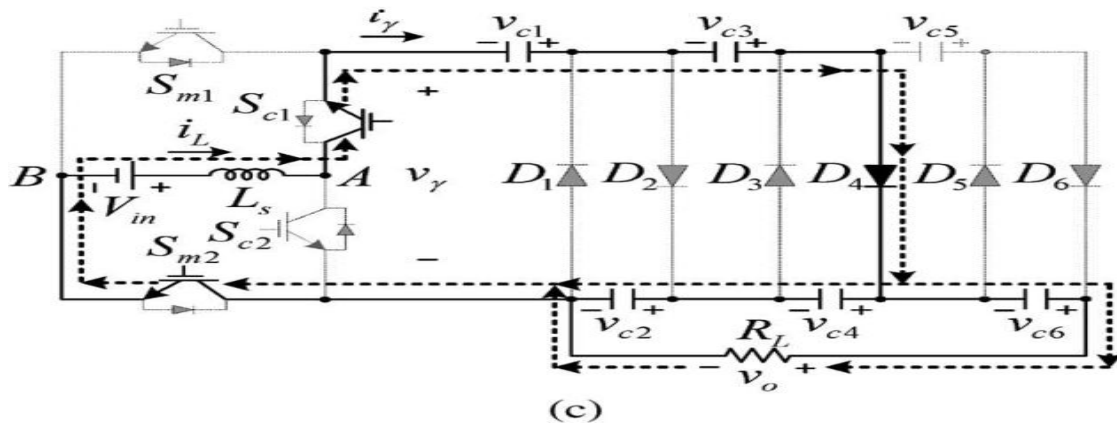
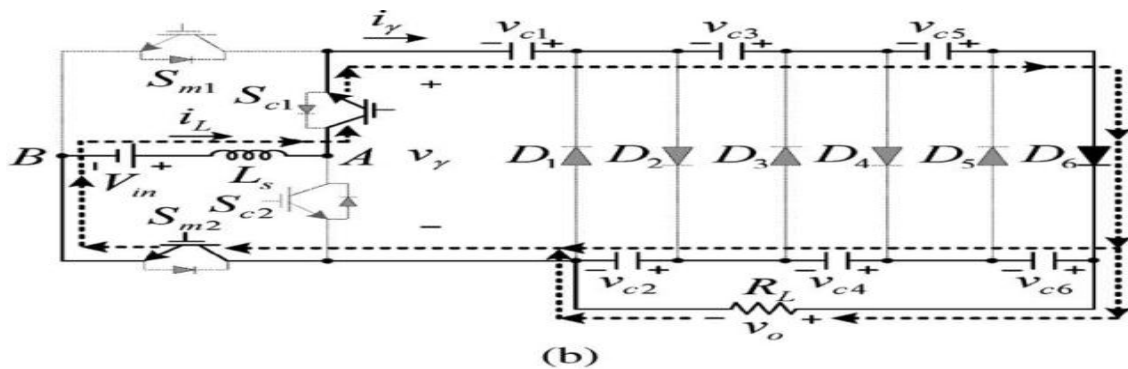


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**Mode 2:**  $S_{m2}$  and  $S_{c1}$  Switches are turned on,  $S_{m1}$  and  $S_{c2}$  Switches are turned off, the current  $i_\gamma$  is positive. The boost inductor ( $L_s$ ) and input  $V_{in}$  dc source are in series the boosted energy transfer to the CW voltage multiplier through different even diodes, mode 2-A, diode  $D_6$  is conducting; the even-group capacitors  $C_6$ ,  $C_4$ , and  $C_2$  are get charged, and the odd-group capacitors  $C_5$ ,  $C_3$ , and  $C_1$  are discharged by  $i_\gamma$ . Is Shown In Fig. (c), mode 2-B, diode  $D_4$  is conducting. Thus,  $C_4$  and  $C_2$  are get charged,  $C_3$  and  $C_1$  are discharged by  $i_\gamma$ ,  $C_6$  supplies load current, and  $C_5$  is floating. Is shown In Fig. (d), mode 2-C, diode  $D_2$  is conducting. Thus,  $C_2$  is charged,  $C_1$  is discharged by  $i_\gamma$ ,  $C_6$  and  $C_4$  supply load current, and  $C_5$  and  $C_3$  are not in conduction.

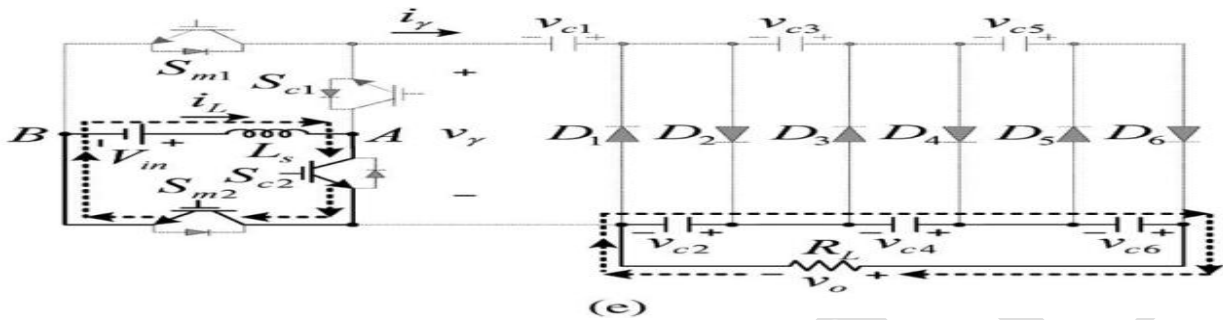


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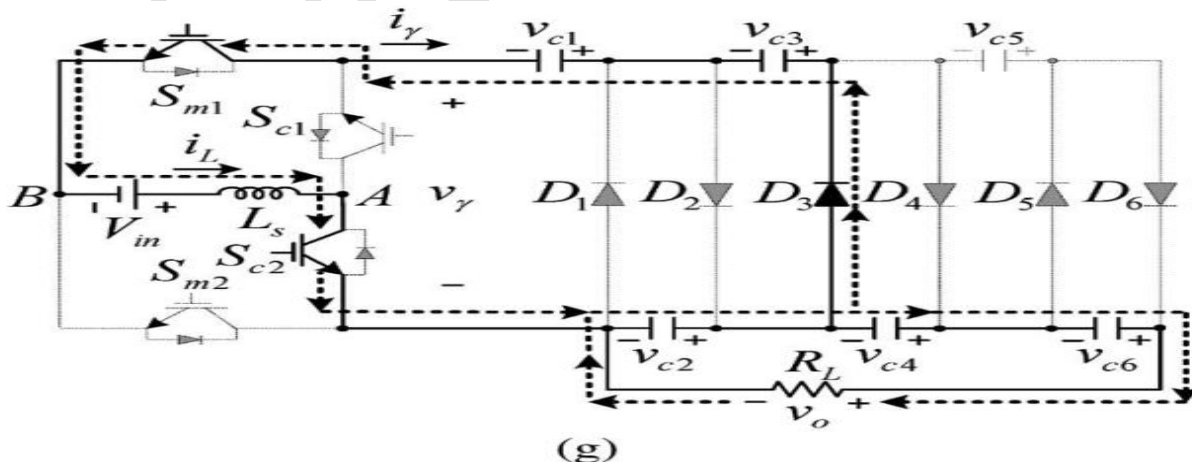
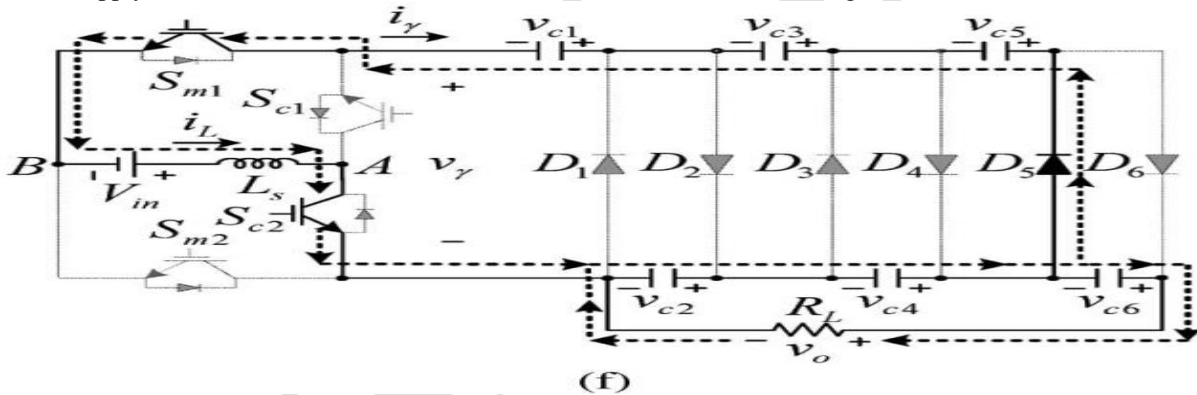
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**Mode 3:** Sm2 and Sc2 Switches are turned on, and Sm1, Sc1, and all CW diodes are turned off, as shown in Fig (e). The boost inductor  $L_s$  is get charged by the  $V_{in}$  dc source, the even group capacitors C6, C4, and C2 supply the load current, and the odd-group capacitors C5, C3, and C1 are not in conduction.



**Mode 4:** Sm1 and Sc2 Switches are turned on, Sm2 and Sc1 Switches are turned off, and the current  $i_\gamma$  is negative. The boost inductor  $L_s$  and input  $V_{in}$  dc source are in series the boosted voltage is “ $-V_\gamma$ ” transfer energy to the CW voltage multiplier through odd diodes, mode 4-A, show in fig (f) diode D5 is conducting. Thus, the even-group capacitors, except C6 which supplies load current, are discharged, and the odd-group capacitors C5, C3, and C1 are charged by  $i_\gamma$ . mode- 4-B, D3 is conducting. Thus, C2 is discharged, C3 and C1 are charged by  $i_\gamma$ , C6 and C4 supply load current, and C5 is not in conduction. Is shown In Fig (g), mode-4-C, D1 is conducting. Thus, C1 is charged by  $i_\gamma$ , all even capacitors supply load current, and C5 and C3 are not in conduction is shown In Fig (h).



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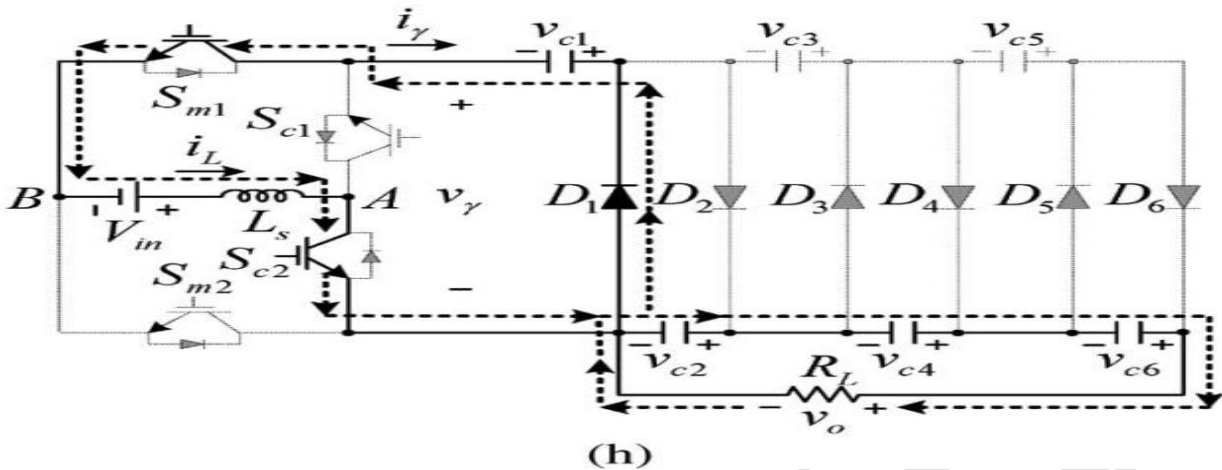


Fig.2. Principle operating modes during one switching period 3-Stage Cockcroft-Walton voltage multiplier operation: (a) for Mode 1. (b),(c)and(d) for Mode 2. (e) for Mode 3. (f), (g) and(h) for Mode 4 operation.

The values and ratings of the components used in simulation circuit is given in table.1

Input Voltage	42-48V	Switching Device's	IGBTs
capacitors (C <sub>1</sub> -C <sub>6</sub> )	470μF	Diodes	PN-junction
Ls	1.5mH	Output Voltage	450V
Switching Frequency(fsc)	1KHZ	Output Current	0.45A
Switching Frequency(fsm)	60KHZ	Output Power	200W

Table. 1 SIMULATION CONFIGURATION

## V. SIMULATION AND RESULT

In this chapter given obtained simulated results are presented for the closed loop analysis of 3-stage Cock-craft Walton (CW) voltage multiplier.



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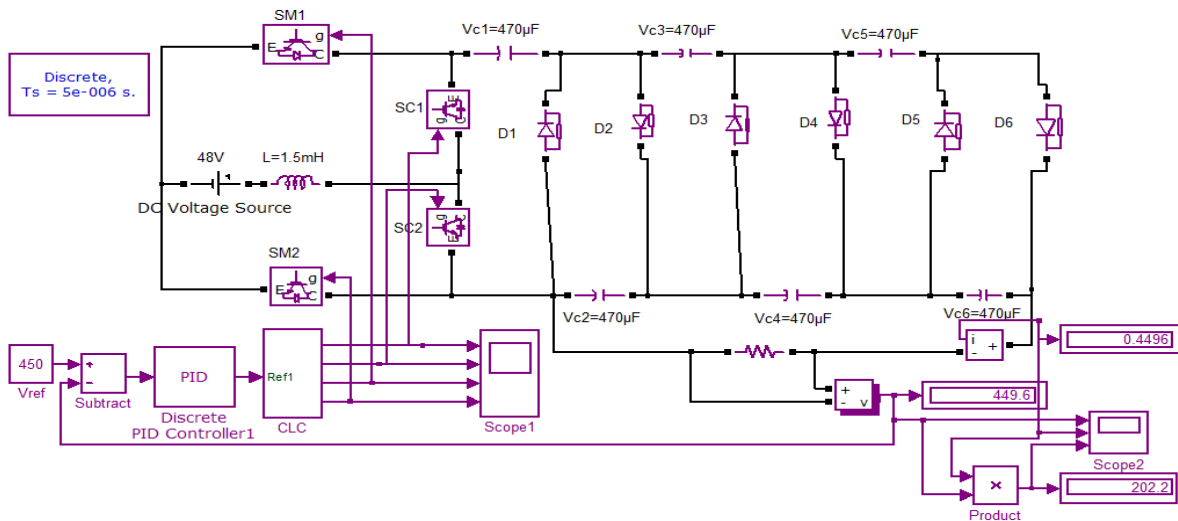
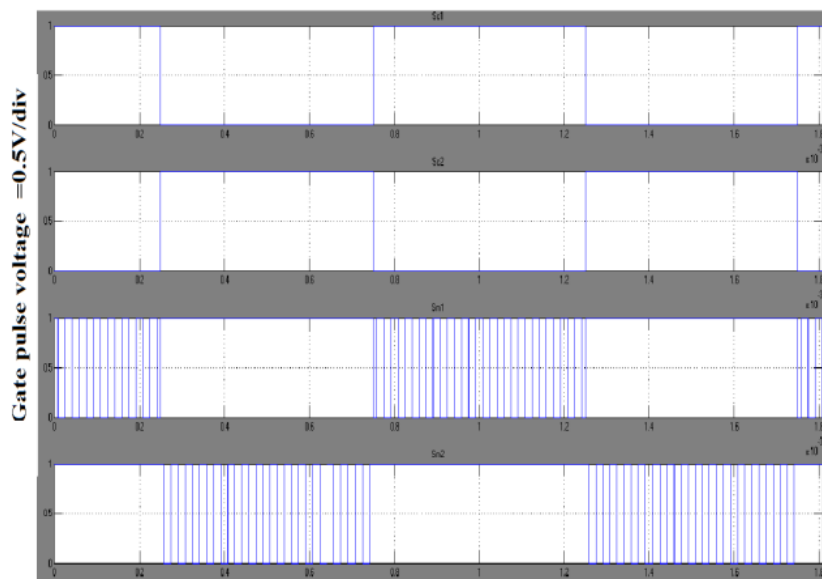


Fig. 3 Simulation circuit for the closed loop 3-Stage cock-craft Walton voltage multiplier

In fig.4 shows the gate pulses for Sc1, Sc2, Sm1, Sm2. When Sc1 is on (1KHZ) Sc2 is off and sm1 is operate at 60KHZ. Similarly when Sc2 (1KHZ) is on Sc1 is off Sm2 operate at 60KHZ.



Time(msec) = 0.2msec/div

Fig. 4 Gate pulses for Sc1, Sc2, Sm1, Sm2.

In fig.5 shows the voltage across the each capacitor. The voltage across the capacitor C1 is less than the half of the remaining capacitors voltage. When odd capacitors (C1, C3, C5) are charging the even capacitors (C2, C4, C6) are discharging. Similarly when even capacitors (C1, C3, C5) are discharging the odd capacitors (C2, C4, C6) are charging. As shown in graph (fig.5), the voltage across all capacitors is almost the same (except C1). We can select all capacitors at the same rating.

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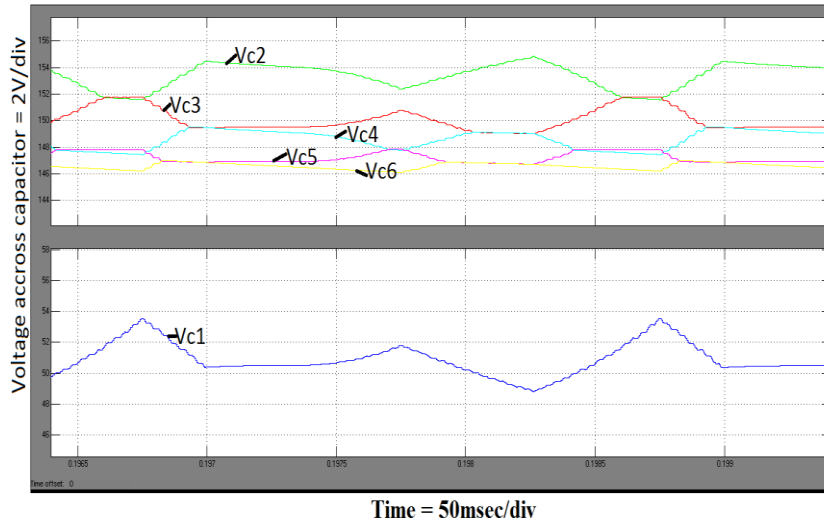


Fig. 5 Voltage across capacitors

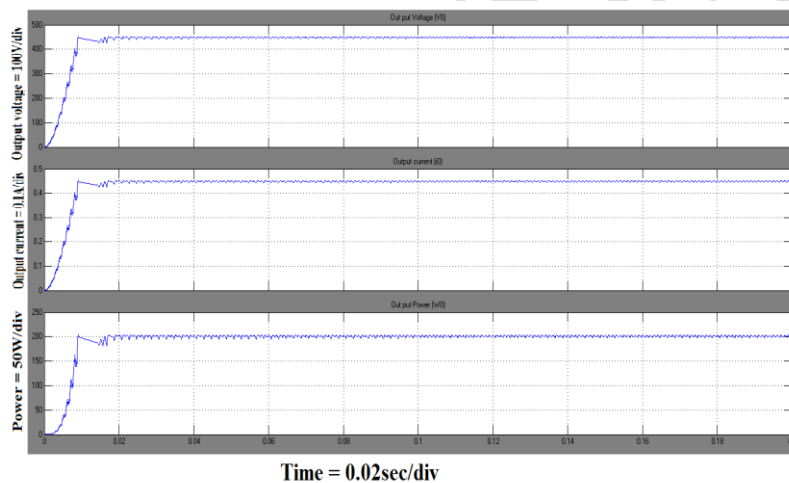


Fig. 6 Output Wave forms for output voltage ( $V_o$ ), output current ( $i_o$ ), Output Power ( $W_o$ )

These are simulated results obtained for the 3-stage Cockcroft-Walton (CW) voltage multiplier. The input voltage for Cockcroft-Walton (CW) generator is 48V, Output voltage is 450V, output current is 0.45Amp, and Output power is 200W. The output voltage range can be increased by adding the number of stages, for every stage we have to connect the two more capacitors and two more diodes.

## VI. CONCLUSION

In this paper, a high step-up dc-dc converter based on the Cockcroft-Walton (CW) voltage multiplier without using a transformer has been presented to obtain a high voltage gain. Since the voltage stress on the active switches, diodes, and capacitors is not affected by increasing the number of cascaded stages, power components with the same voltage ratings can be selected. The Control strategy employs two independent frequencies, one is operates at high frequency to minimize the size of the inductor ( $L_s$ ) while the other one operates at relatively low frequency according to the desired output voltage ripple. Finally, the simulation and experimental results proved the validity of theoretical analysis and the feasibility of the proposed converter. In future we can increase number of n-stages the high dc output voltage can be converted to AC voltage.



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